



Università di Pisa

Corso di Laurea Magistrale in Ingegneria Biomedica

***Development of a fast high fidelity FSI  
workflow to simulate polymeric aortic valves:  
a RBF mesh morphing study***

Relatori:

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*Prof. Marco Evangelos Biancolini*

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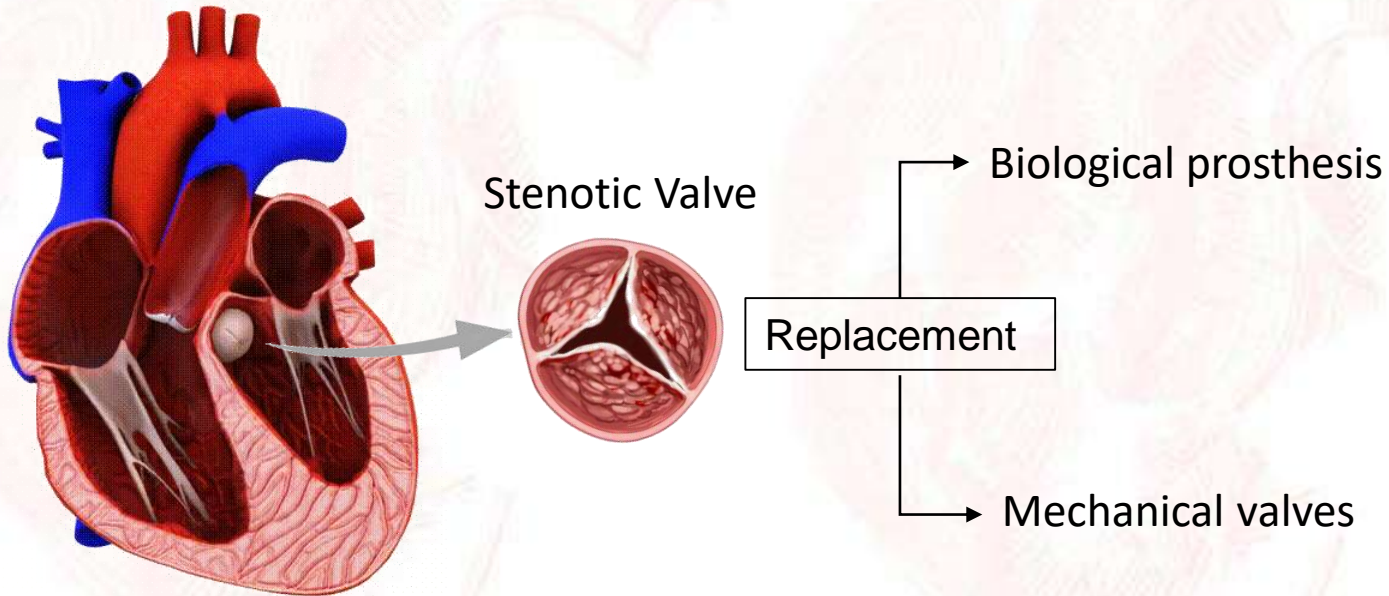
Candidato:

*Leonardo Geronzi*

A. A. 2018/2019

2018: cardiovascular diseases are the first cause of death in the world [1]

→ Aortic Stenosis: shrinkage of the aortic orifice



## Polymeric-Prosthetic Heart Valves (P-PHVs)



- Crimpable
- Less inclined to coagulation problem
- Customizable
- Easy to be produced
- Cheap

Currently, FDA<sup>2</sup> and ASME<sup>3</sup> are forcing on the advancement and widespread adoption of new approaches based on numerical simulation which require better computational tools that are fast, accessible and individually adaptable

[2]

The screenshot shows the FDA website header with the logo and 'U.S. FOOD & DRUG ADMINISTRATION'. Below the header is a breadcrumb trail: 'Home / Medical Devices / Device Advice: Comprehensive Regulatory Assistance / Reprocessing of Reusable Medical Devices: Information for Manufacturers / Computational Modeling: A Proposed Simulation Tool for Designing Reusable Medical Devices for Reprocessing'. The main title of the page is 'Computational Modeling: A Proposed Simulation Tool for Designing Reusable Medical Devices for Reprocessing'.

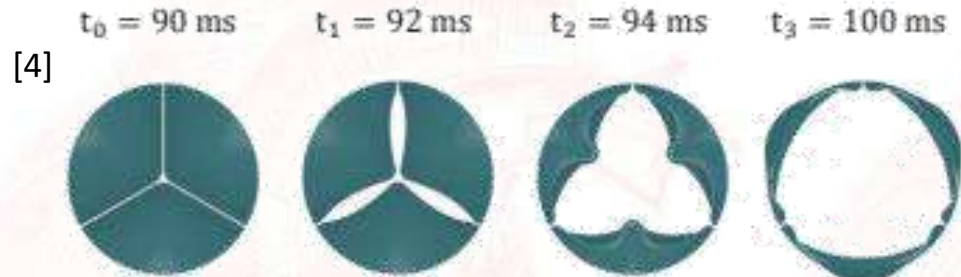
[3]

The screenshot shows the ASME website header with the logo and 'The American Society of Mechanical Engineers'. Below the header is a navigation menu with links for 'About ASME', 'Codes & Standards', 'Certification & Accreditation', 'Learning & Development', and 'Publications & Submissions'. The breadcrumb trail is 'Codes & Standards > Find Codes & Standard > V V 40 Assessing Credibility of Compu...'. The main title of the page is 'Assessing Credibility of Computational Modeling through Verification and Validation: Application to Medical Devices' and the version is 'V V 40 - 2018'.

[2] U.S. Food & Drug Administration

[3] American Society of Mechanical Engineers

## Structural simulations



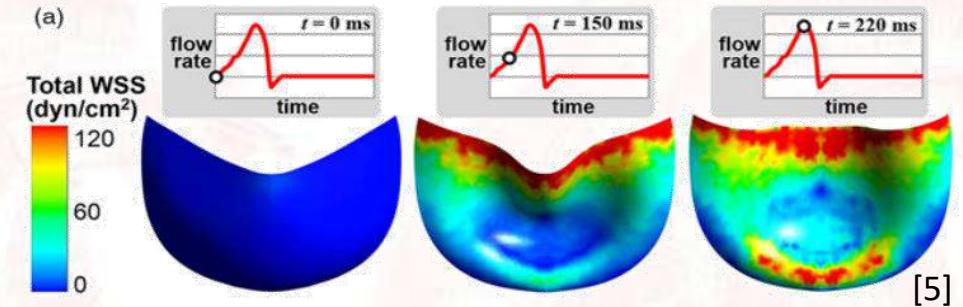
### Output parameters:

- Equivalent von-Mises stress
- Equivalent strain
- Maximum displacement
- Maximum Geometric Orifice Area ( $GOA_{max}$ )
- Maximum Coaptation Area ( $CA_{max}$ )



High computational time to solve simulations

## Fluid-Structure Interaction (FSI) analysis



### Output parameters:

- Wall Shear Stress (WSS)
- Volumetric Flow Rate (VFR)

$$\tau_w = \mu \left( \frac{\partial u}{\partial y} \right)_{y=0} = 32\mu \frac{Q}{\pi d^3}$$

Development of a novel numerical approach able to reduce computational time with *fast-high fidelity*

*Coupling between FSI and mesh morphing techniques*

Generation of a new upgradable and adaptable parametric model of the aortic valve

Influence of parameters with respect to output values

Method for changing the shape of a surface, preserving its topology: nodal positions are only updated

## Based on Radial Basis Functions (RBF)

To interpolate in the space a scalar function  $s(x)$  defined at discrete points, giving the exact values at original points

$$s(x) = \sum_{i=1}^N \gamma_i \varphi(\|x - x_{s_i}\|) + h(x)$$

$$h(x) = \beta_1 + \beta_2 x + \beta_3 y + \beta_4 z$$



3D-space

$$\begin{cases} s_x(x) = \sum_{i=1}^N \gamma_i^x \varphi(\|x - x_{s_i}\|) + \beta_1^x + \beta_2^x x + \beta_3^x y + \beta_4^x z \\ s_y(x) = \sum_{i=1}^N \gamma_i^y \varphi(\|x - x_{s_i}\|) + \beta_1^y + \beta_2^y x + \beta_3^y y + \beta_4^y z \\ s_z(x) = \sum_{i=1}^N \gamma_i^z \varphi(\|x - x_{s_i}\|) + \beta_1^z + \beta_2^z x + \beta_3^z y + \beta_4^z z \end{cases}$$

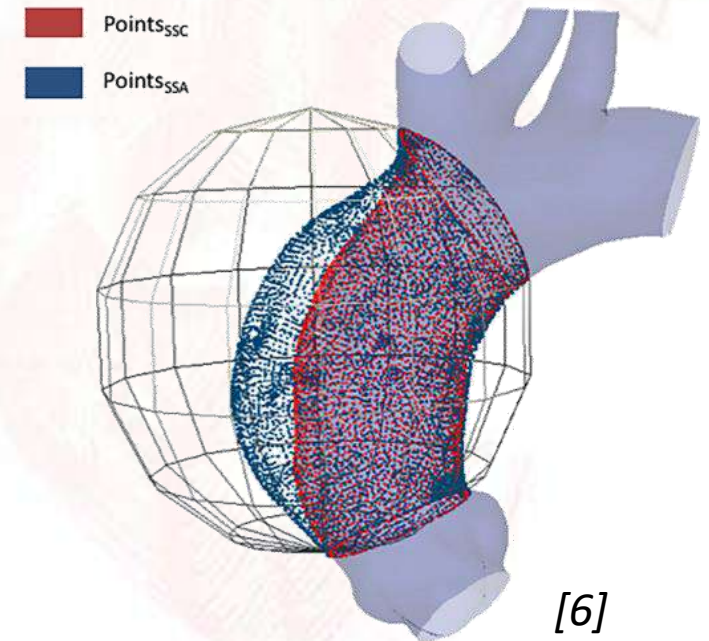
$\gamma_i$ : weights of the model

$\varphi(\cdot)$ : RBF

$x$ : generic position

$x_{s_i}$ : source point

$h(x)$ : polynomial term



## 1. Valve design

- Python & SpaceClaim

## 2. Structural analysis

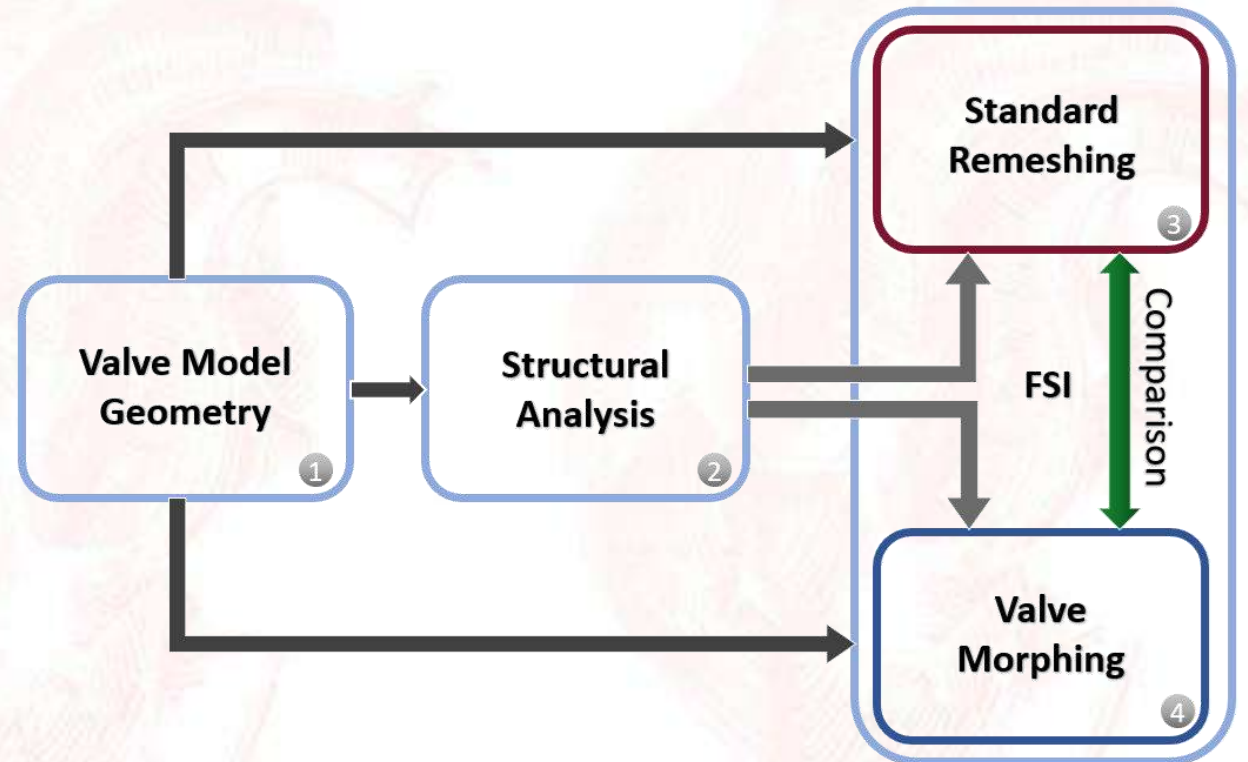
- Ansys Workbench Mechanical

## 3. Remeshing – FSI

- Ansys Workbench Mechanical & Fluent System Coupling

## 4. *Morphing – FSI*

- *Fluent & RBF Morph Add-On*



Parametric model

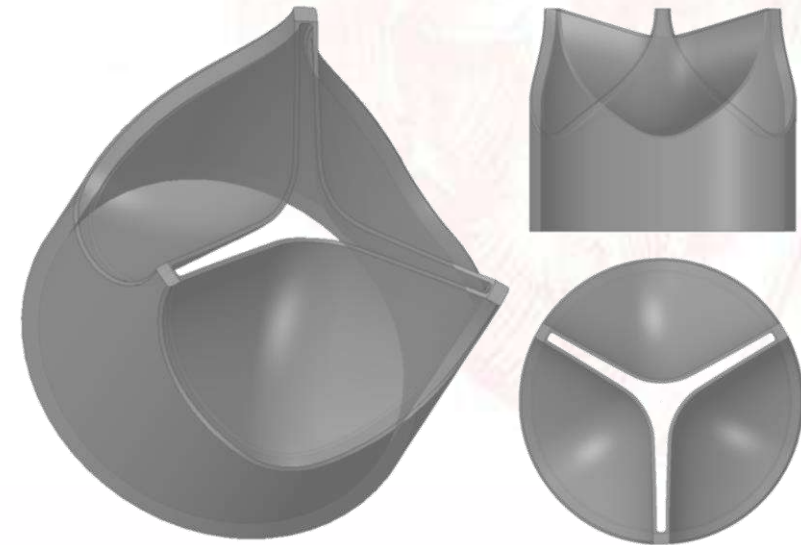
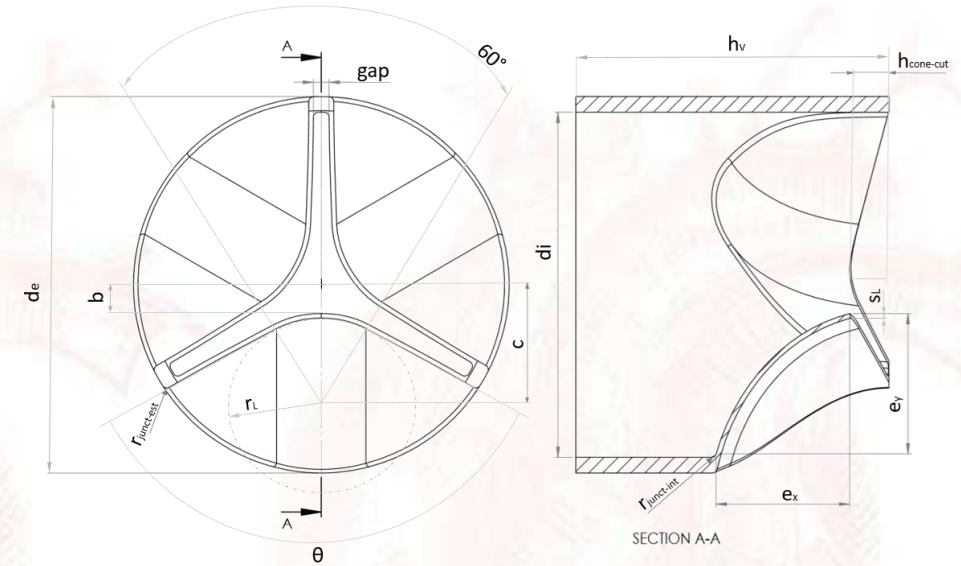


Identification of a surgical candidate

Design parameters

FIXED\*

Parameter	Meaning	Value
$r_e$	External radius of the circular ring	Fixed: 12 mm
$r_i$	Internal radius of the circular ring	Fixed: 11 mm
$\theta$	Revolution angle of the leaflets	Fixed: 120°
$s_l$	Thickness of the leaflets	Fixed: 0,3 mm
$h_v$	Height of the whole valve	Fixed: 20 mm
$e_x$	Ellipse-x parameter for the entrainment	Parametrized
$e_y$	Ellipse-y parameter for the entrainment	Parametrized
$r_l$	Radius of the internal arc which defines the upper surface of the leaflet	Parametrized
$g$	Semi-gap between one leaflet and the other one in proximity to the ring	Parametrized
$r_{junct-est}$	Junction radius between the external face of the leaflet and the ring	Parametrized
$r_{junct-int}$	Junction radius between the internal face of the leaflet and the ring	Parametrized
$h_{cone-cut}$	Maximum internal cutting height to generate Lunula angle of the valve	Parametrized



\*@ patient specific level



Parametric model

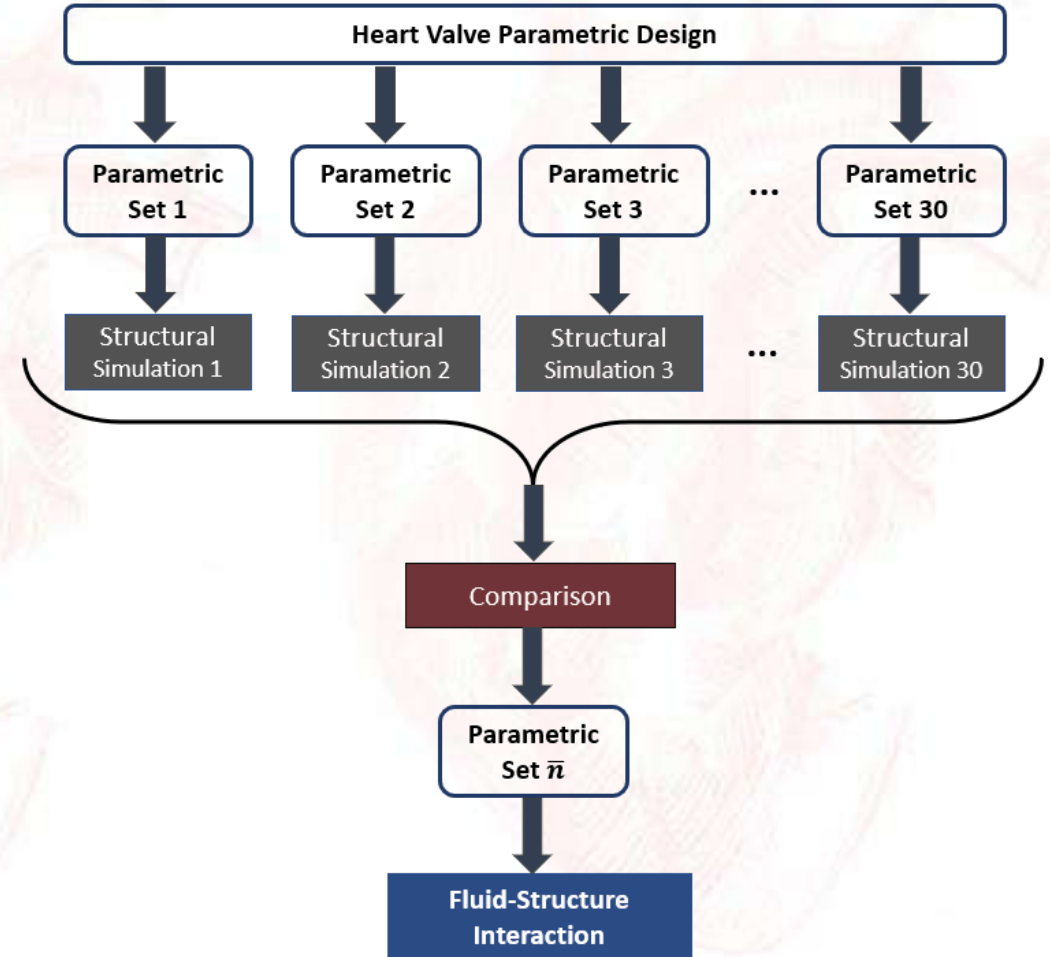


Identification of a surgical candidate

Design parameters

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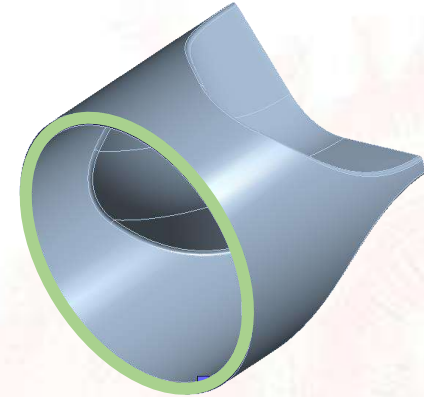
FIXED\*



\*@ patient specific level

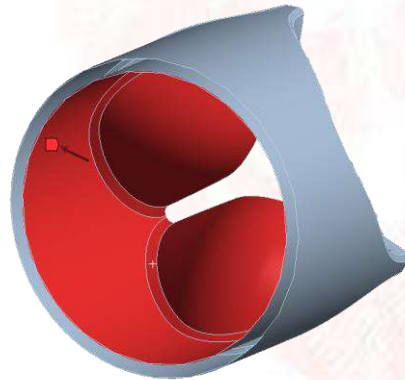
## ANSYS Mechanical

- Material properties: isotropic linear elastic ( $E = 3 \text{ MPa}$ ,  $\nu = 0.4$ )
- Element type: tetrahedral (from 237533 to 368730)
- Boundary condition: **bottom surface** of the circular **ring fixed in displacement**



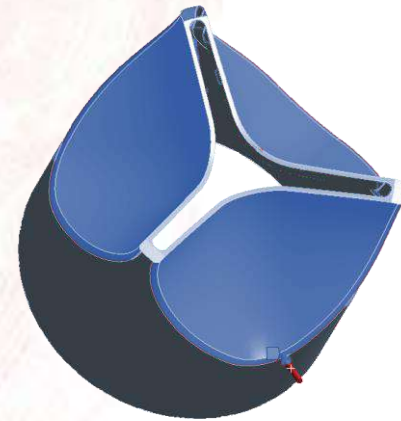
## Opening

- 15 opening simulations ( $O_1$ - $O_{15}$ )
- Transvalvular systolic pressure



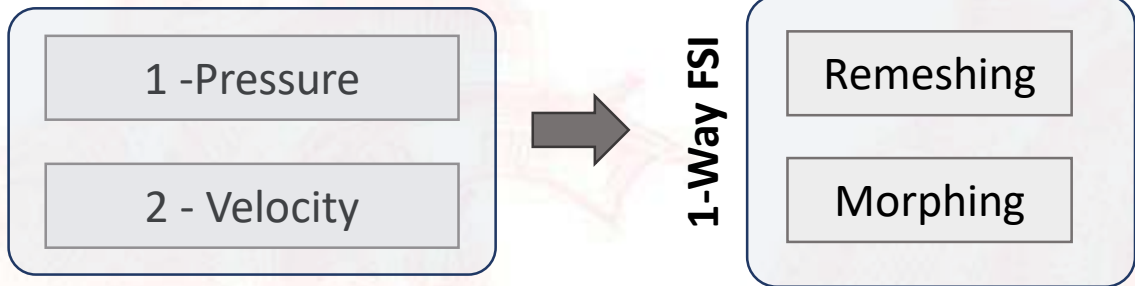
## Closing

- 15 closing simulations ( $C_1$ - $C_{15}$ )
- Transvalvular diastolic pressure

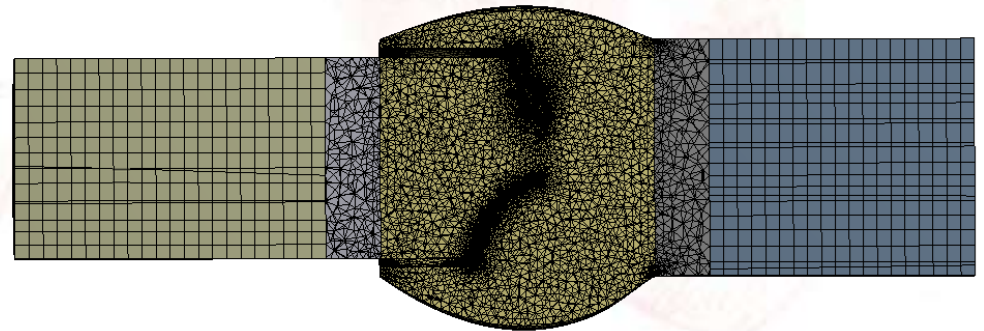
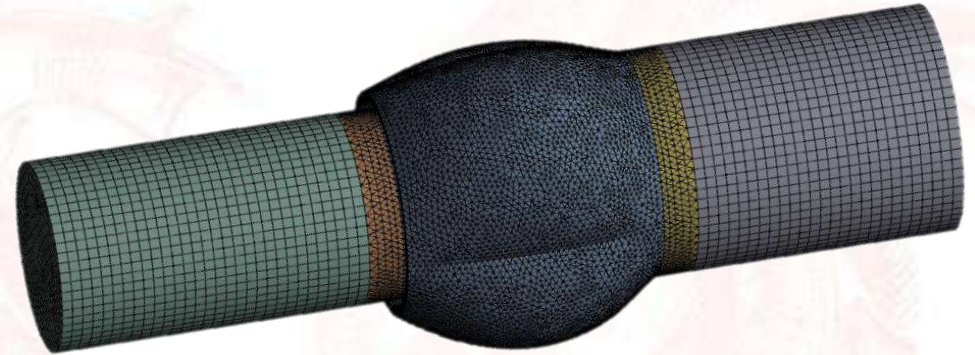


- From structural analysis: Parametric set 15

Two inlet boundary conditions



Tetra-hexahedral Mesh

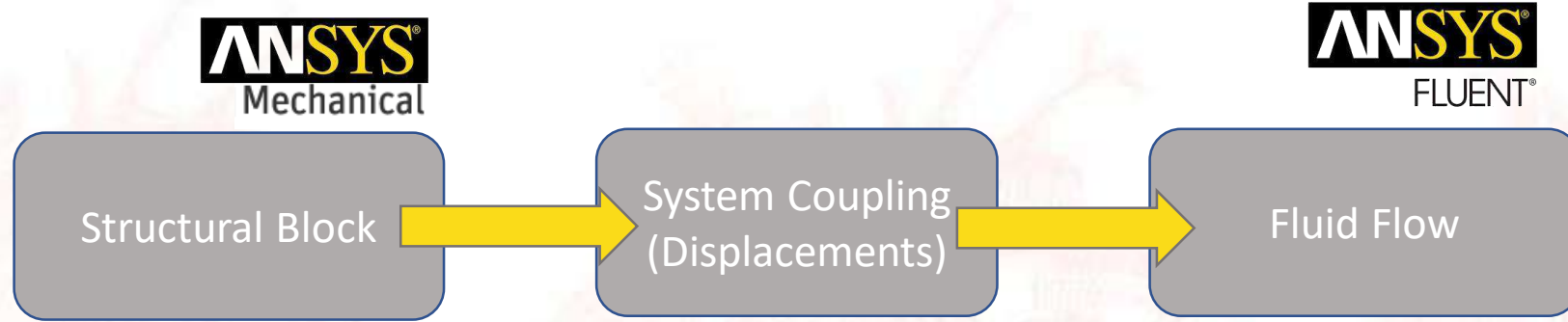


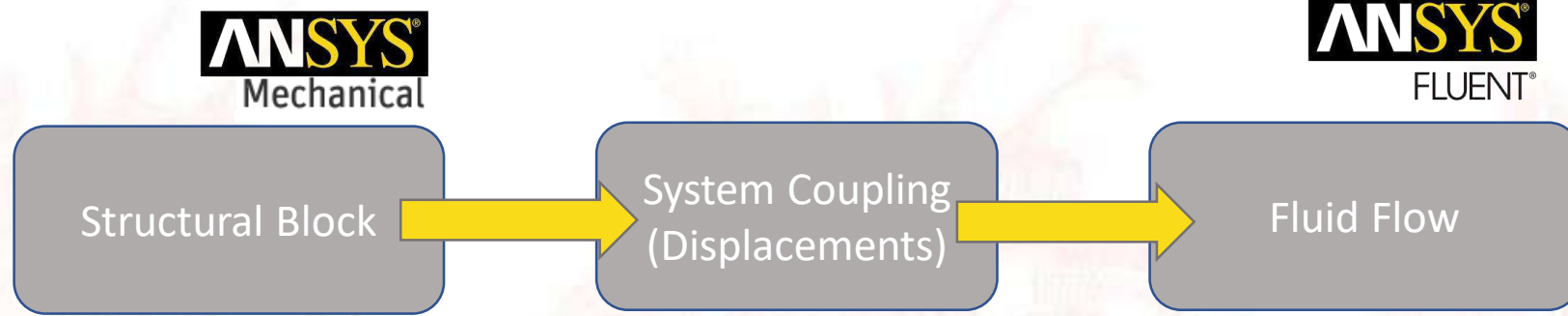
## Fluid Setting:

- Newtonian fluid ( $\mu = 4$  cP) Viscous-Laminar
- $\rho = 1000$  kg/m<sup>3</sup>
- Number of elements 1.5 million
- Time step=  $1e-5$  s
- Simulation time= 14 ms

## Structural Setting:

- Number of elements 0.5 million
- Transvalvular systolic pressure @ ventricular side





Dynamic meshing tools:

- 1) Spring-Based Smoothing
- 2) **Remeshing**

## Starting conditions

- Maximum starting Skewness=0.694
- Minimum element length=0.1 mm
- Maximum element length=1.8 mm

*Remeshing if*

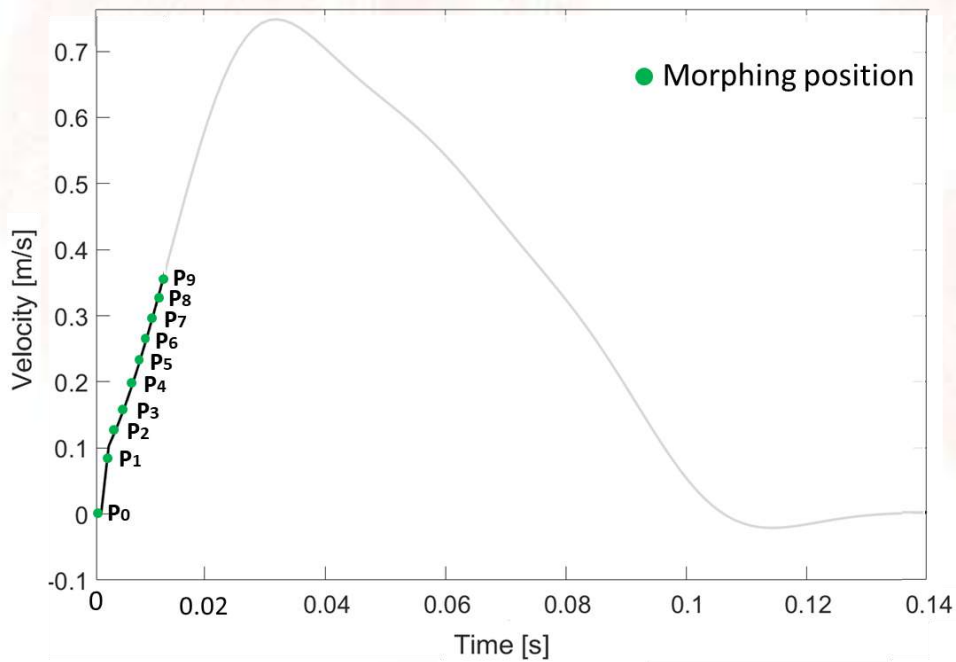


## Limit conditions

- Skewness > 0.72
- Minimum element length < 0.06 mm
- Maximum element length > 2.5 mm

First strategy – one single direction of morphing

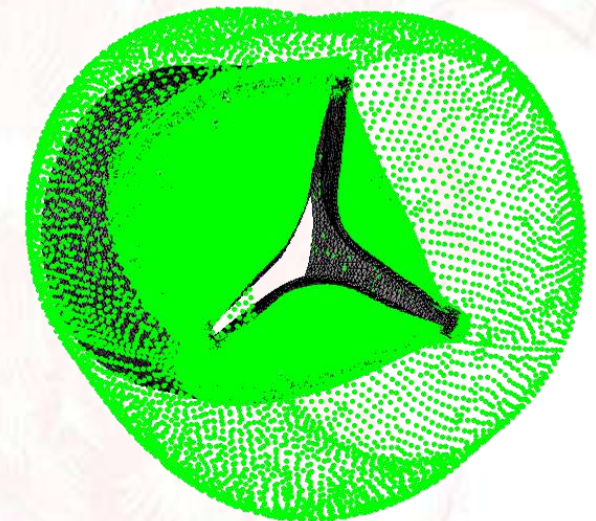
Source and Target points extracted with M-APDL by sampling the valve displacement every 3 mm



Source points



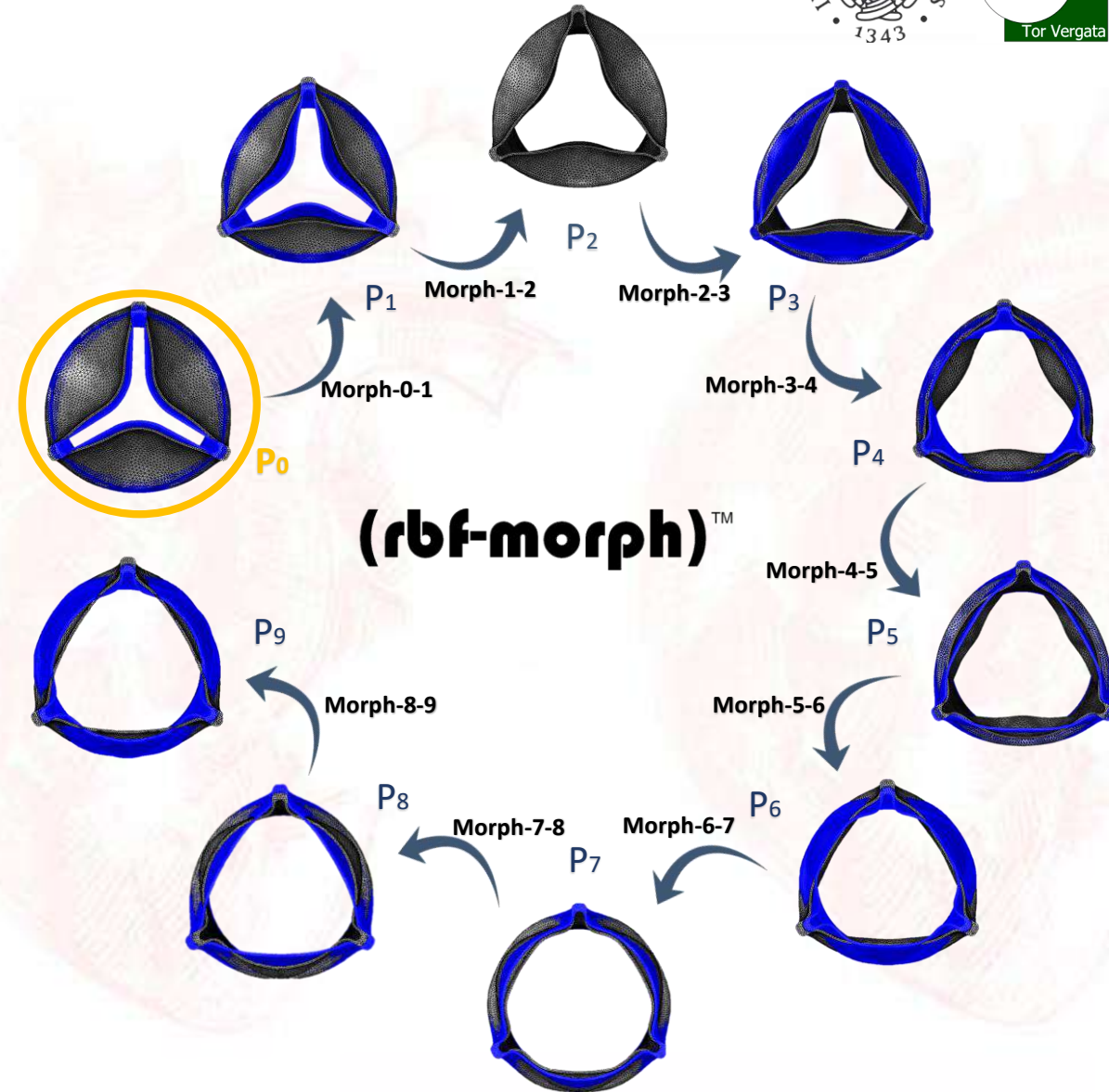
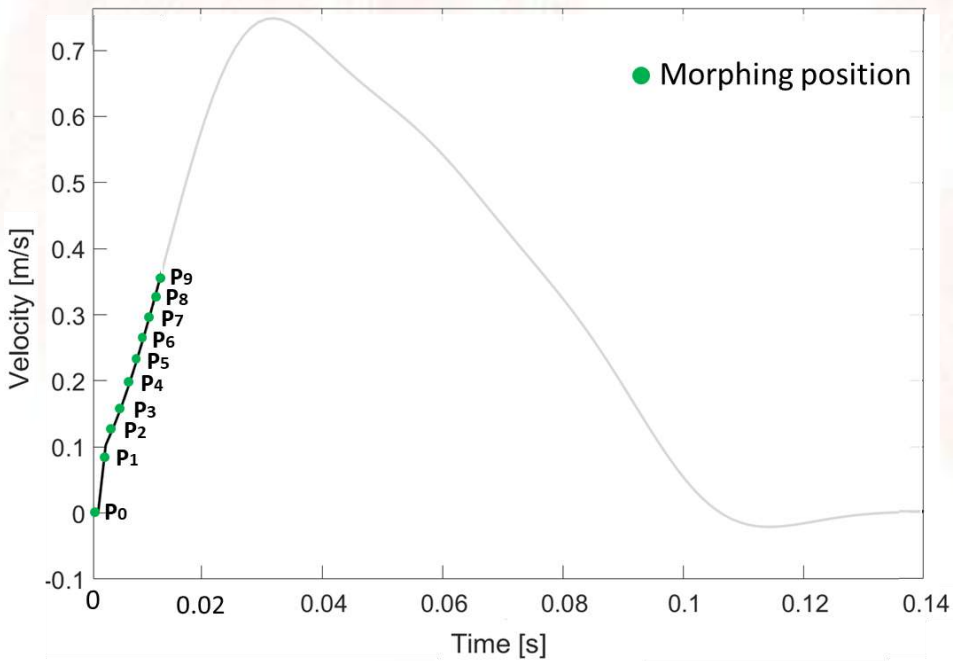
Target points



RBF:  $\varphi(r)=r$

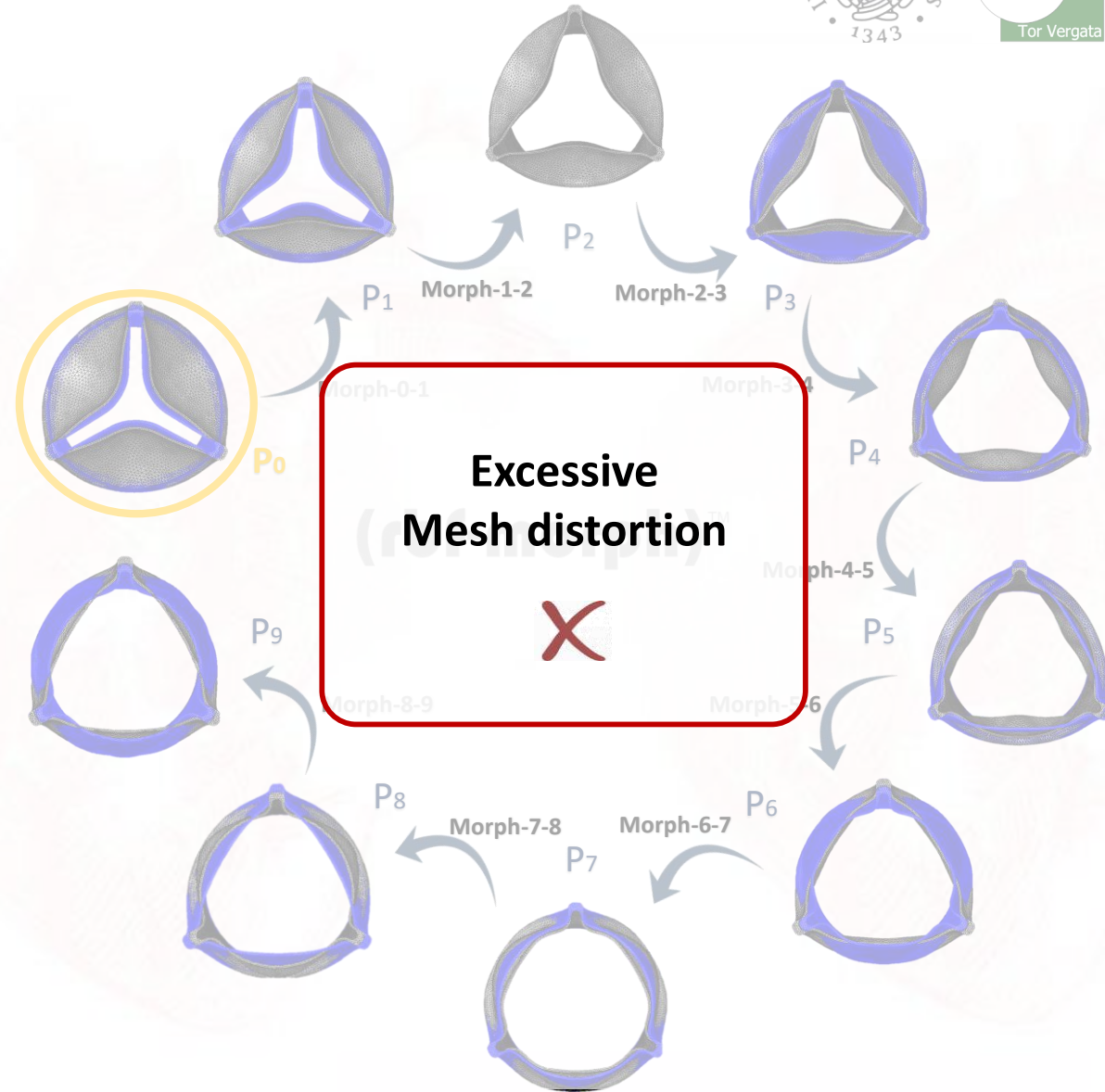
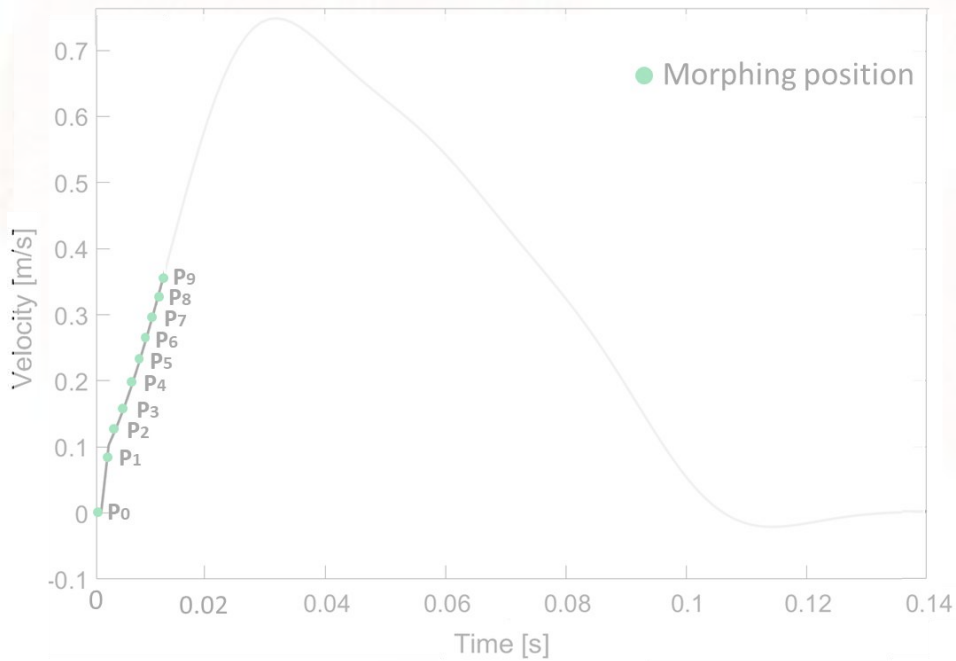
First strategy – one single direction of morphing

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First strategy – one single direction of morphing

Source and Target points extracted with M-APDL by sampling the valve displacement every 3 mm

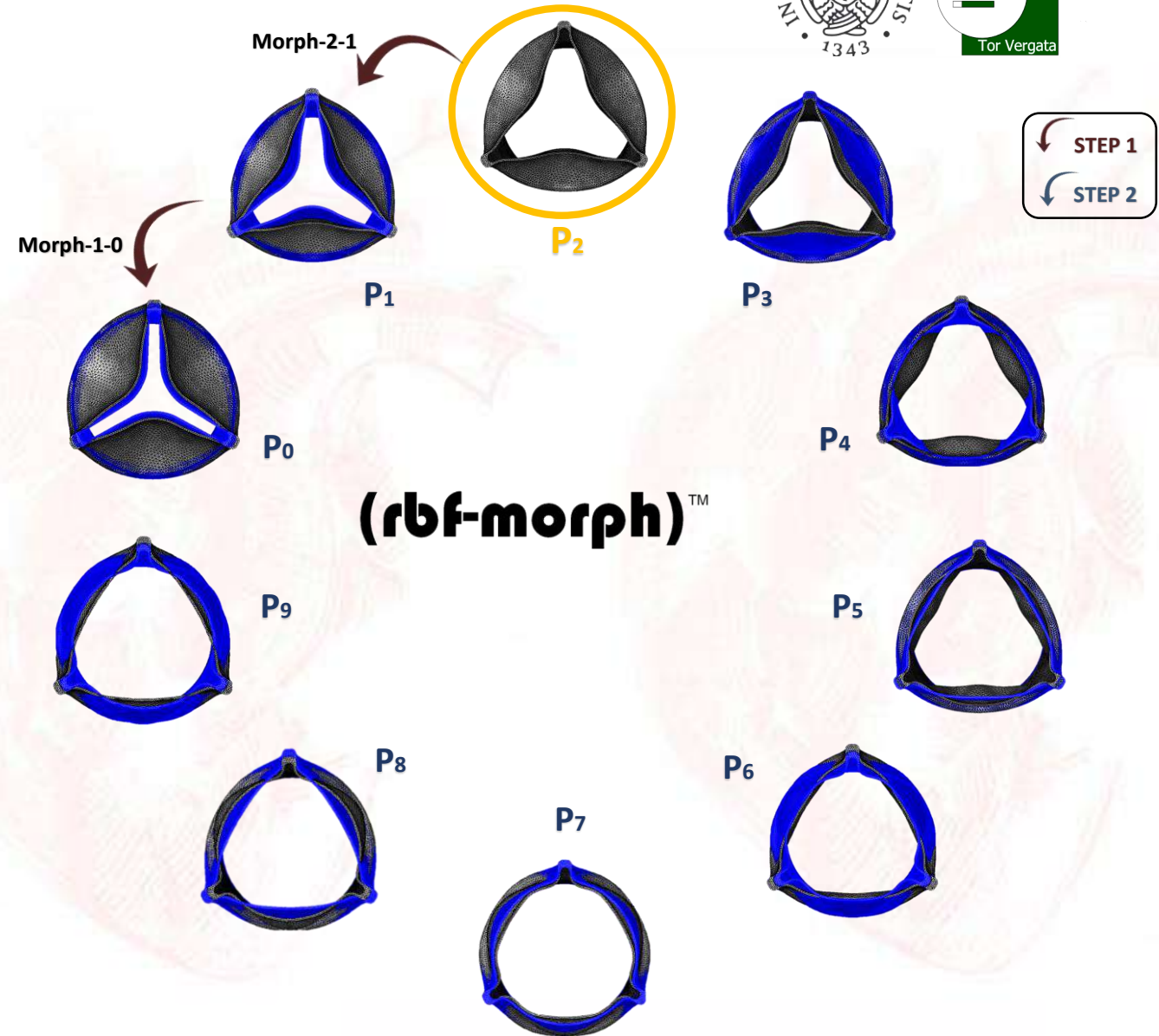




## New morphing procedure

### Step 1: from $P_2$ to $P_0$

- To reach initial position
- Saving of the mesh with a deformation already in place
- Initialization of the flow



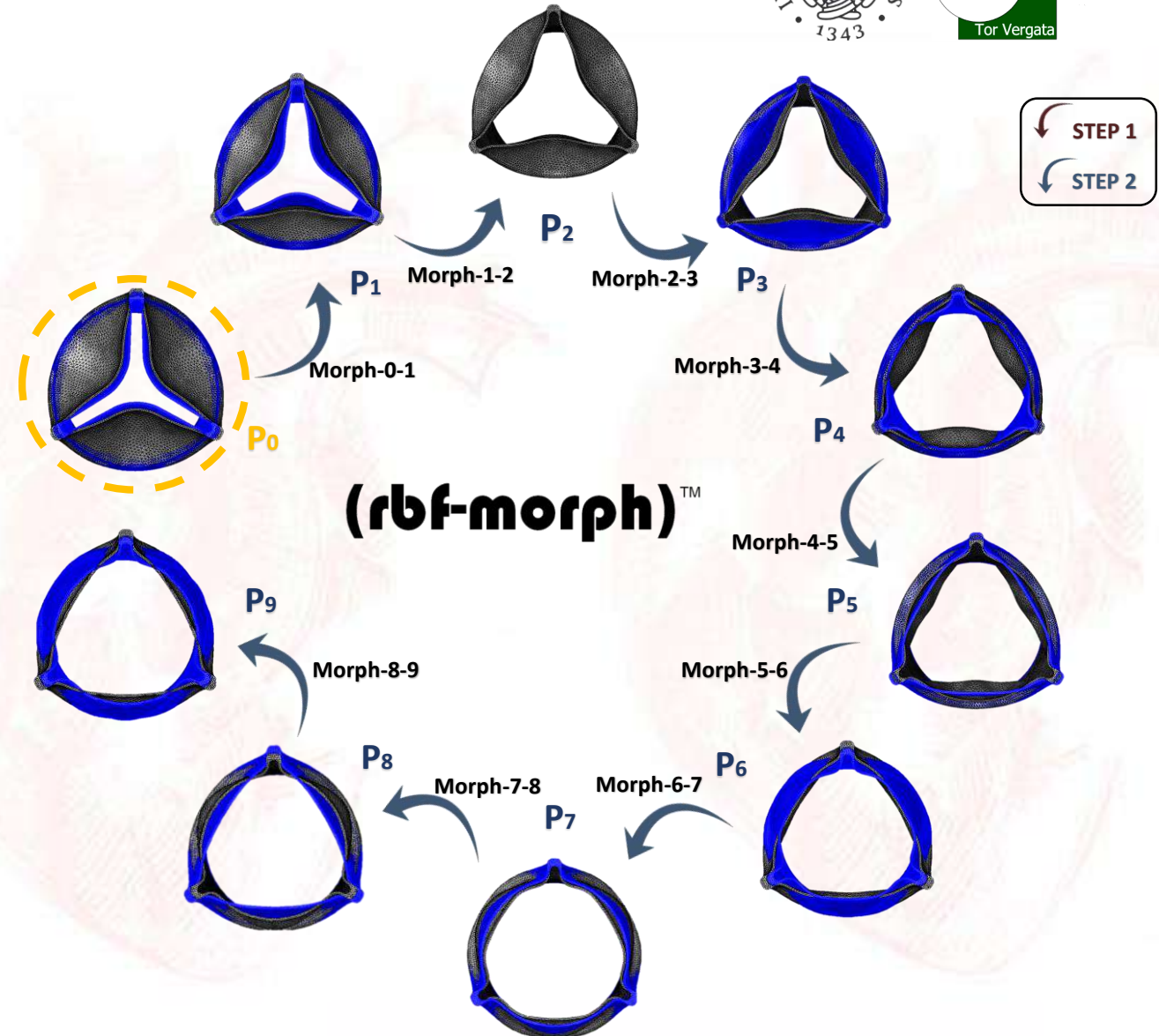
## New morphing procedure

### Step 1: from $P_2$ to $P_0$

- To reach initial position
- Saving of the mesh with a deformation already in place
- Initialization of the flow

### Step 2: from $P_0$ to $P_9$

- To morph all the opening of the valve



## New morphing procedure

### Step 1: from $P_2$ to $P_0$

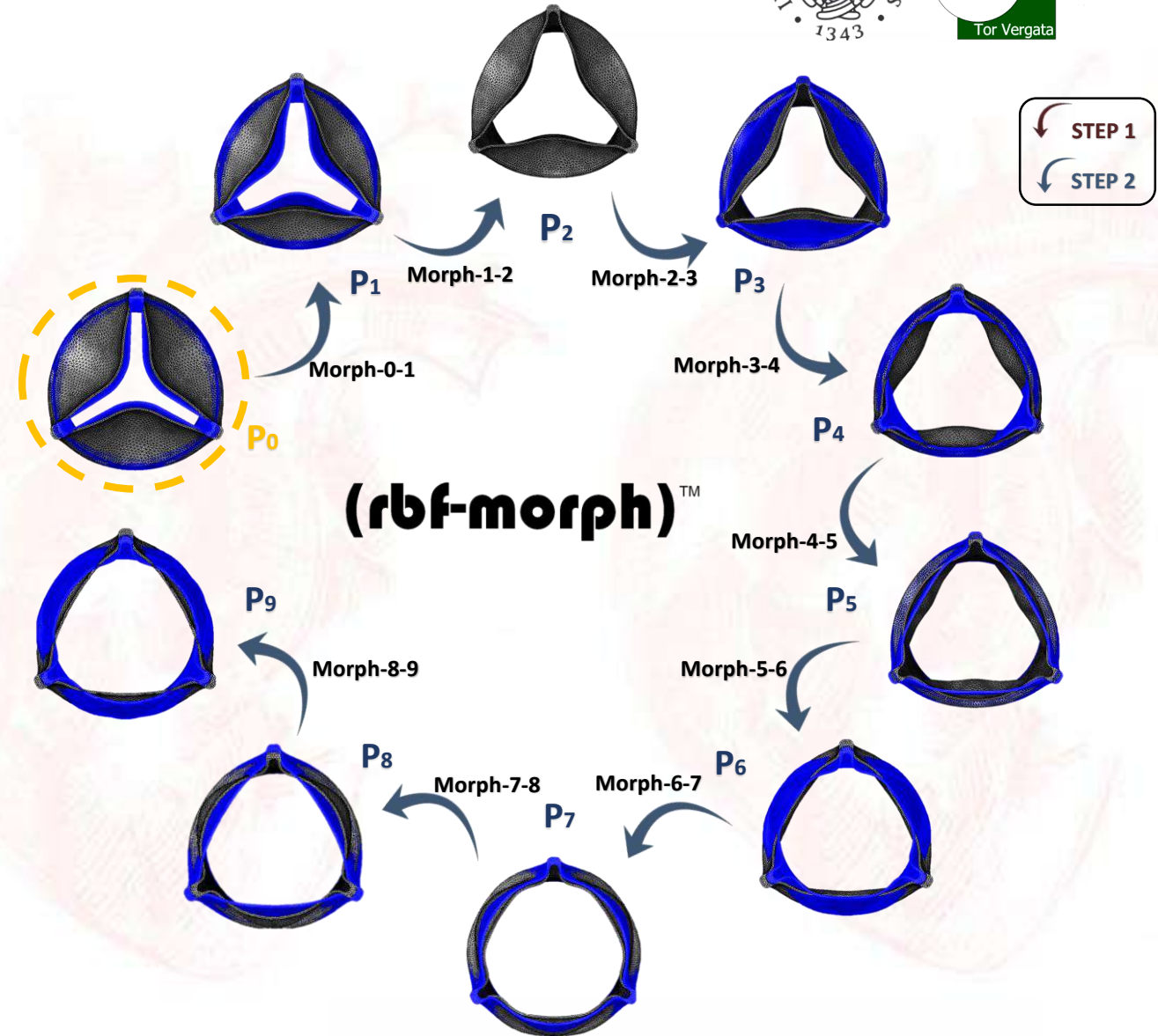
- To reach initial position
- Saving of the mesh with a deformation already in place
- Initialization of the flow

### Step 2: from $P_0$ to $P_9$

- To morph all the opening of the valve

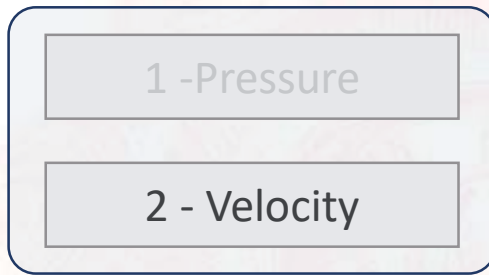
### Scheme program

$$A_0(t) = \begin{cases} 0, & \text{if } t = 0 \\ \left(\frac{t}{t_1}\right)^2, & \text{if } 0 < t < t_1 \\ 1, & \text{if } t \geq t_1 \end{cases} \quad A_i(t) = \begin{cases} 0, & \text{if } t \leq t_i \\ \frac{t-t_i}{t_{i+1}-t_i}, & \text{if } t_i < t < t_{i+1} \\ 1, & \text{if } t \geq t_{i+1} \end{cases}$$

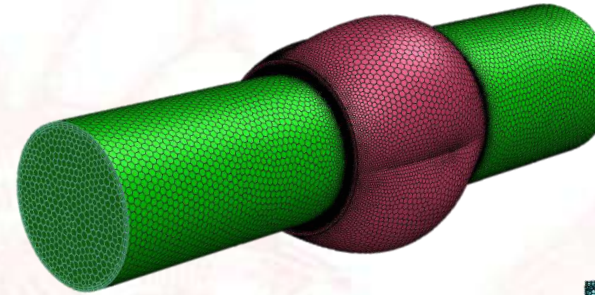


## Complete opening simulation

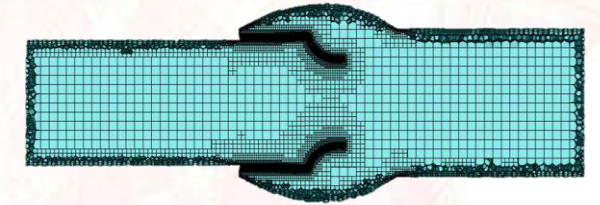
Only one inlet boundary condition



1-Way FSI



Poly-hexahedral Mesh

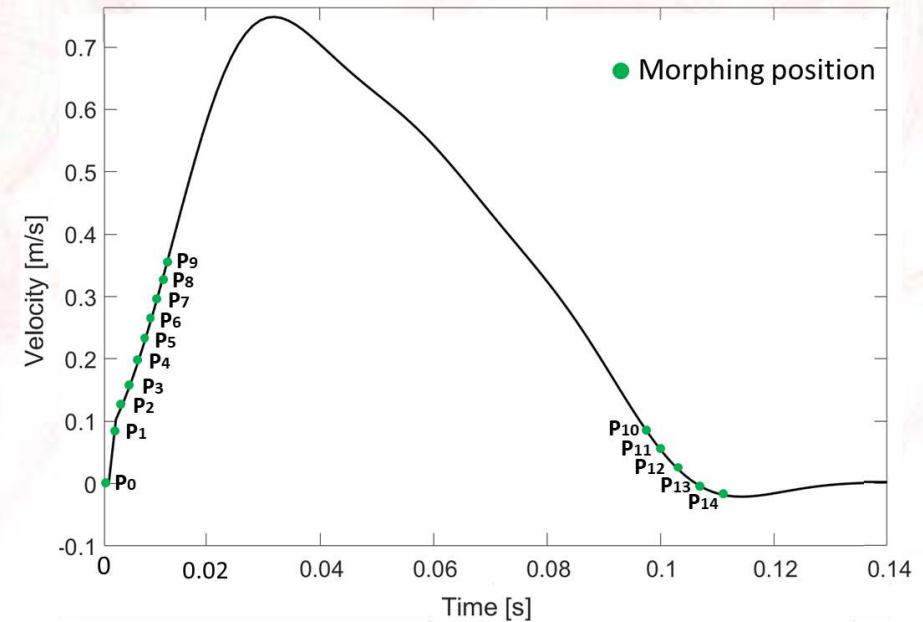


### Fluid Setting:

- Newtonian fluid ( $\mu = 4$  cP) Viscous-Laminar
- $\rho = 1000$  kg/m<sup>3</sup>
- Number of elements 0.9 million
- Time step= 5e-5 s
- Simulation time: 110 ms

### Structural Setting:

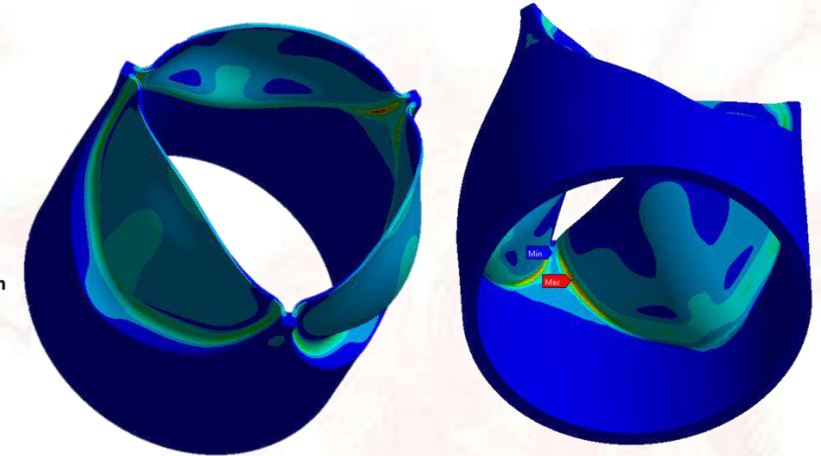
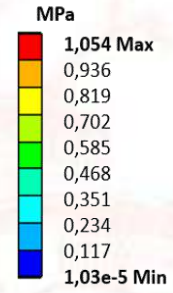
- Number of elements 0.5 million
- Transvalvular systolic pressure @ ventricular side

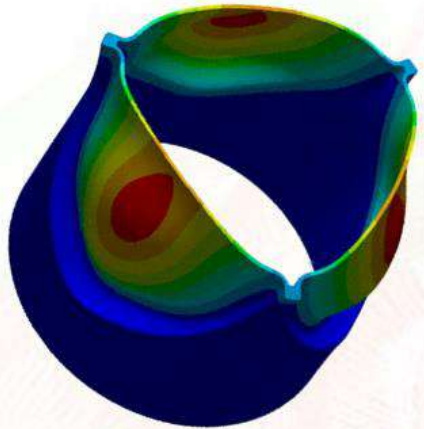




## Opening O<sub>15</sub>

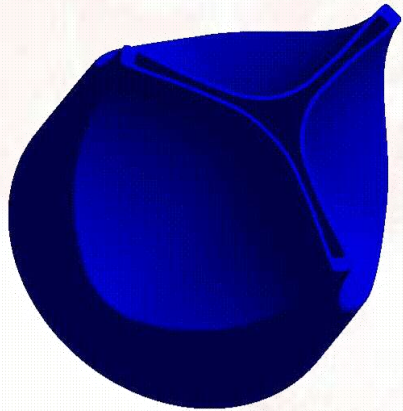
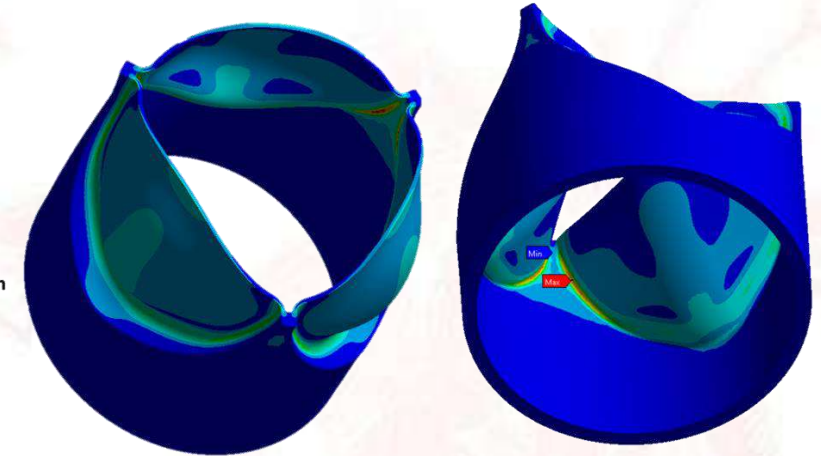
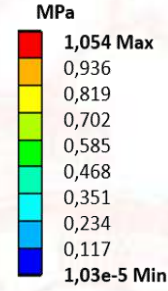
- Maximum eq. von-Mises stress: 1.05 MPa
- Maximum eq. strain: 0.344
- Maximum displacement: 8.74 mm
- GOA<sub>max</sub>: 363.6 mm<sup>2</sup> [7]





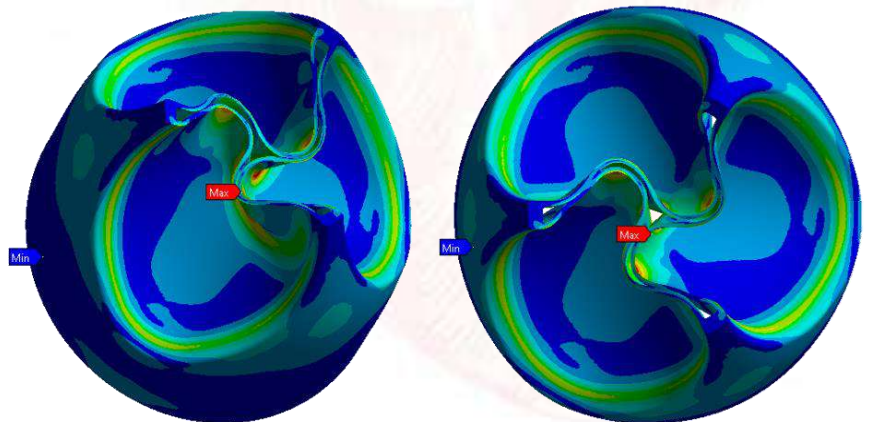
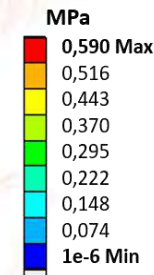
## Opening O<sub>15</sub>

- Maximum eq. von-Mises stress: 1.05 MPa
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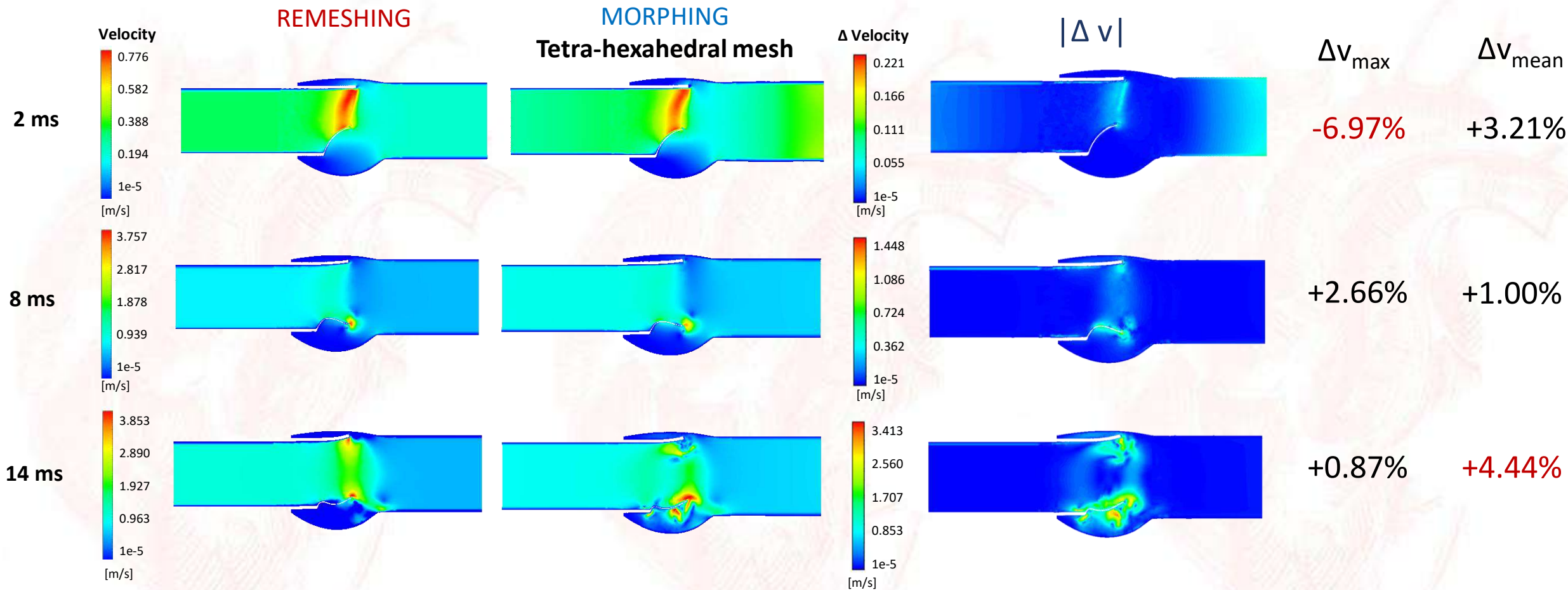


## Closing C<sub>15</sub>

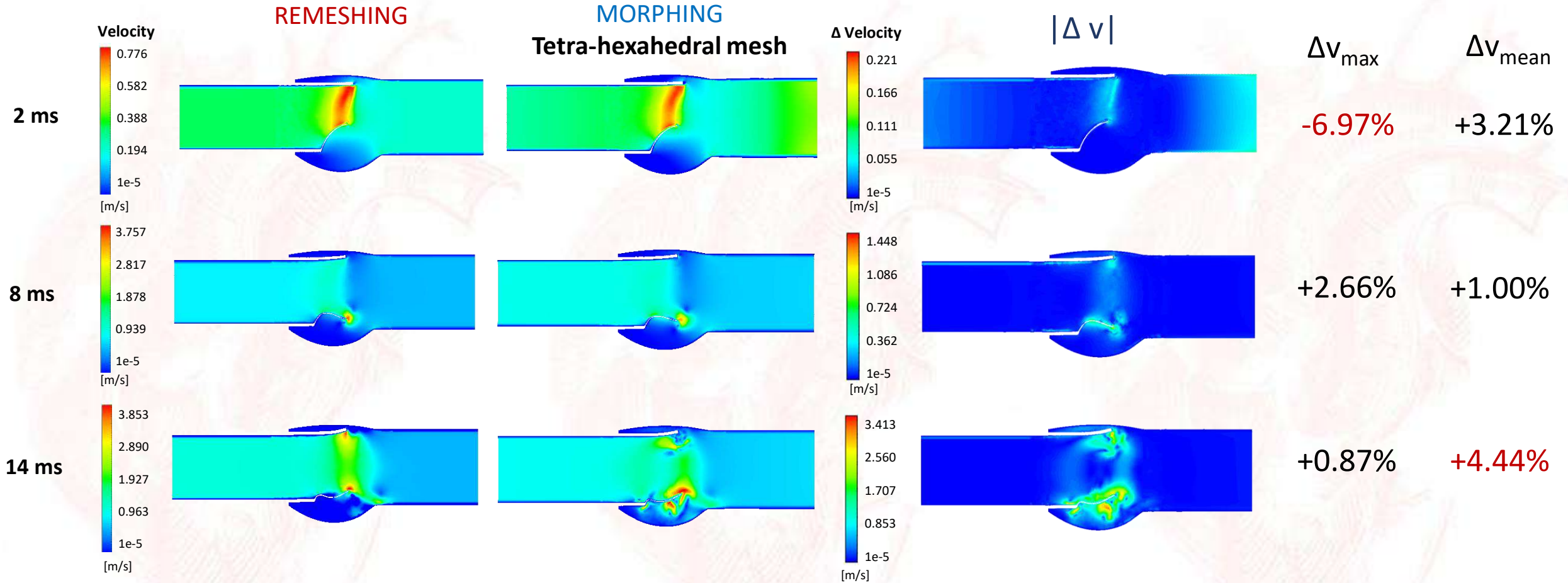
- Maximum eq. von-Mises stress: 0.59 MPa
- Maximum eq. strain: 0.21
- Maximum displacement: 6.18 mm
- CA<sub>max</sub>: 28.6 mm<sup>2</sup> [8]



# Results – Pressure inlet FSI



# Results – Pressure inlet FSI



Computational time

Remeshing: 6283 minutes

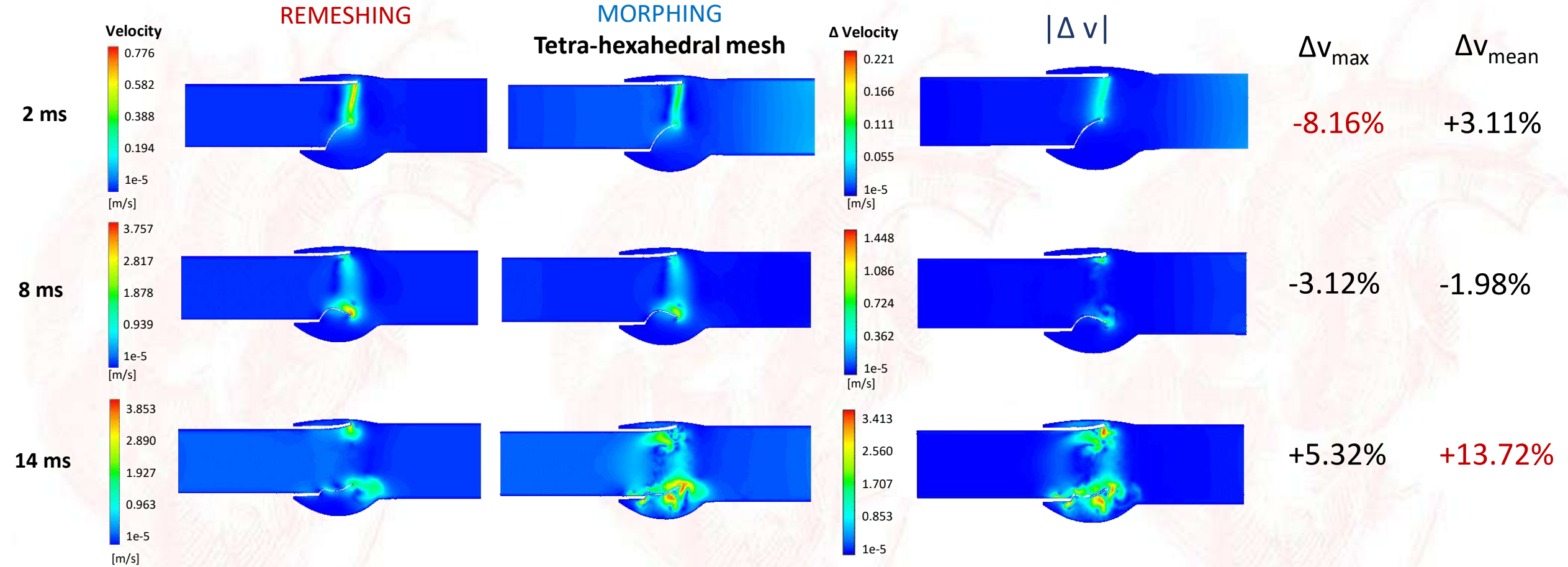
Morphing: 396 minutes



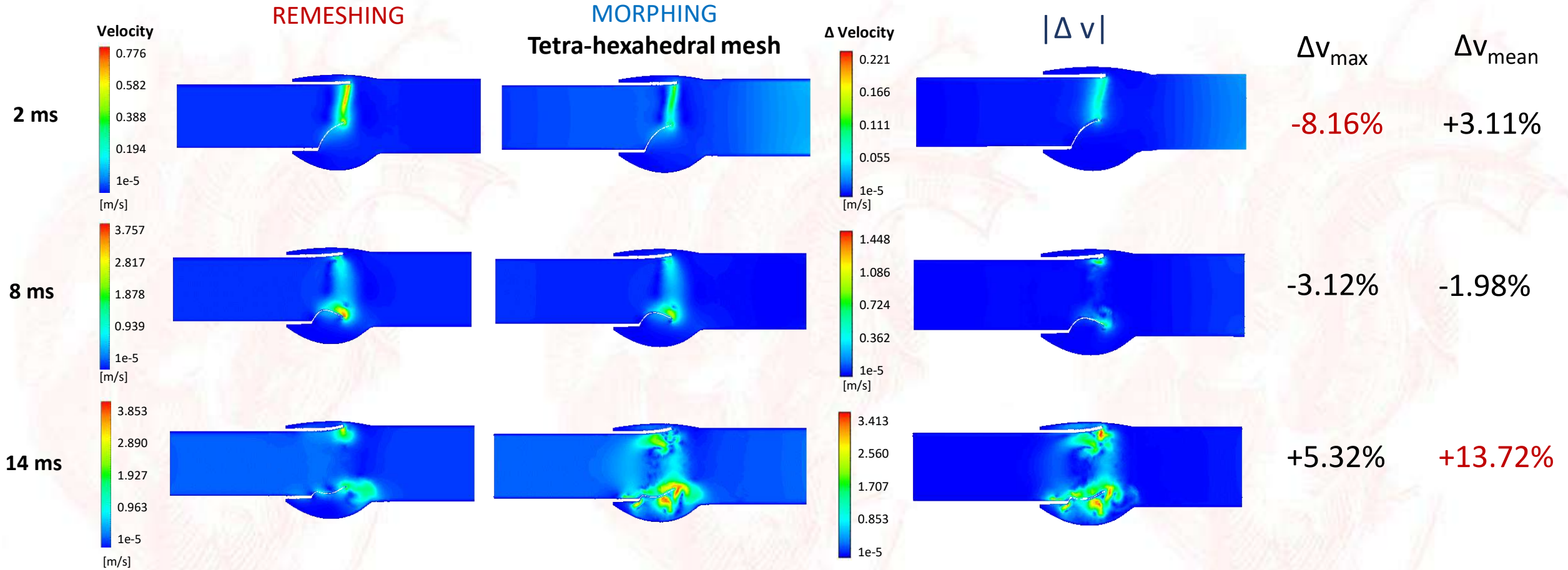
16 times faster



# Results – Velocity inlet FSI



# Results – Velocity inlet FSI



Computational time

Remeshing: 7211 minutes

Morphing: 475 minutes



15 times faster

## REMESHING

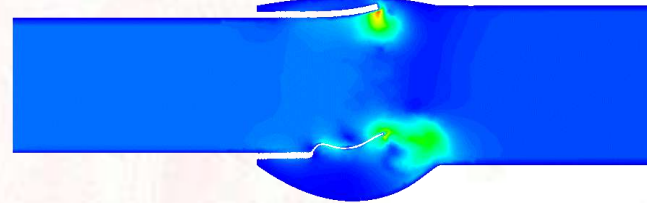
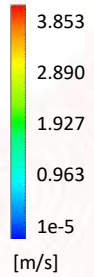
## MORPHING

### Tetra-hexahedral mesh

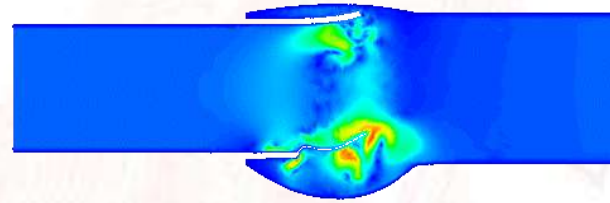
## MORPHING

### Poly-hexahedral mesh

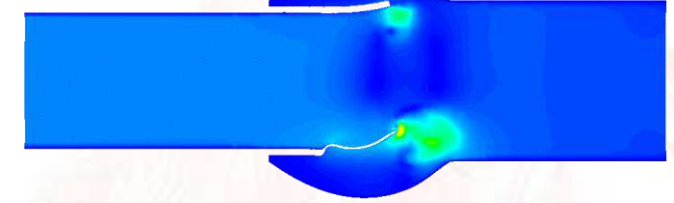
14 ms



Max Velocity 3.891 m/s  
Mean Velocity 0.401 m/s



Max Velocity 3.688 m/s  
Mean Velocity 0.456 m/s



Max Velocity 3.683 m/s  
Mean Velocity 0.403 m/s

$\Delta v_{\max}$

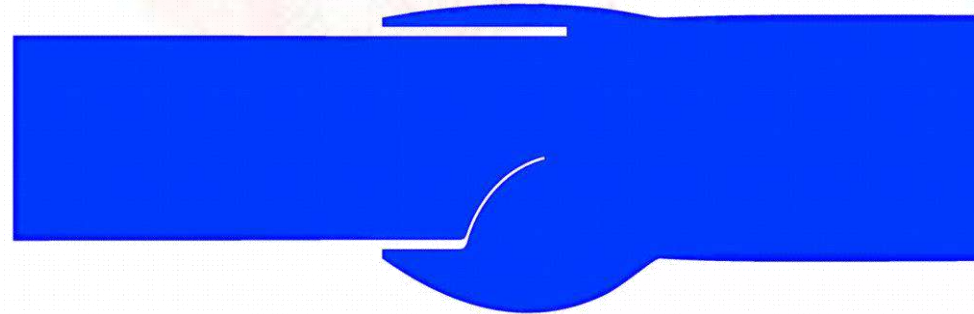
-5.32%

-5.35%

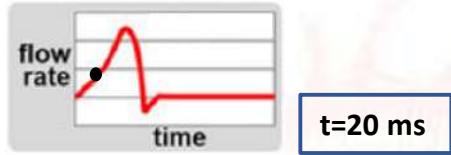
$\Delta v_{\text{mean}}$

+13.72%

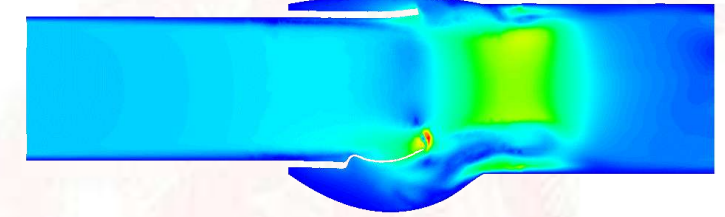
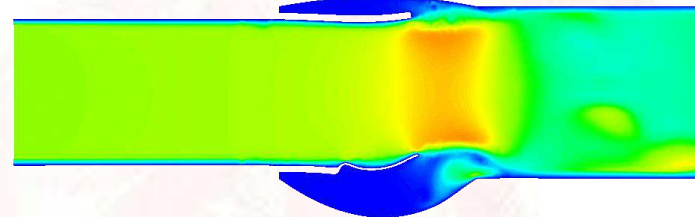
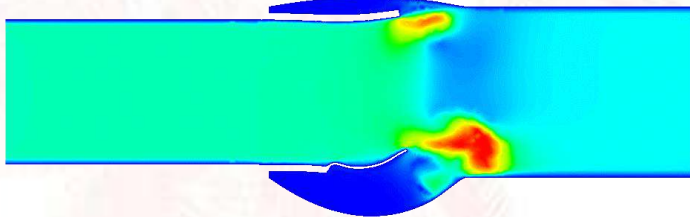
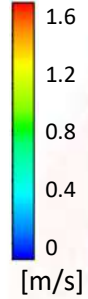
+0.50%



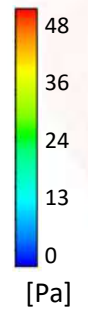
# Results – Full opening FSI



Velocity

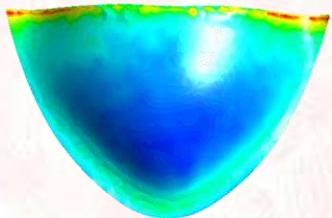


WSS



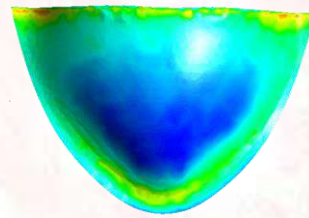
Ventricularis Surface

Aortic Surface



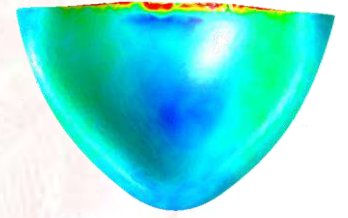
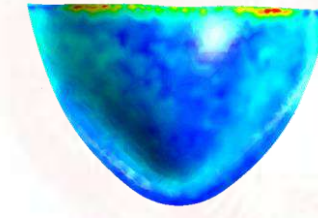
Ventricularis Surface

Aortic Surface



Ventricularis Surface

Aortic Surface



$$WSS_{\max} = 47.58 \text{ Pa}$$

$$WSS_{\text{mean}} = 6.99 \text{ Pa}$$

$$WSS_{\max} = 47.64 \text{ Pa} \quad [9]$$

$$WSS_{\text{mean}} = 7.46 \text{ Pa} \quad [10]$$

$$WSS_{\max} = 46.12 \text{ Pa}$$

$$WSS_{\text{mean}} = 7.51 \text{ Pa}$$

[9] Cao et al., Computer methods in biomechanics and biomedical engineering. 19(6):603–613, 2016.

[10] Burwash, Journal of Biomechanics. 9(2):92–99, 2014.

- High fidelity workflow to solve FSI simulations faster than 15 times in comparison to standard remeshing procedures with similar results
- Based on a parametric patient-specific heart valve design
- Output values consistent with State of the Art

## Future developments

- Implementation of a 2-Way FSI (remeshing and morphing)
- Closing FSI simulation

*Towards a complete cardiac cycle...*



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**Thank you for the attention**