



UNIVERSITY OF LEEDS

# TESI DI LAUREA MAGISTRALE INGEGNERIA MECCANICA

**Goal driven multi-objective shape optimization for conjugate heat transfer in an effusion cooling system of a combustion chamber, through a CFD-mesh-morphing based approach.**

*Relatore*

Prof. Marco E. Biancolini

*Correlatore*

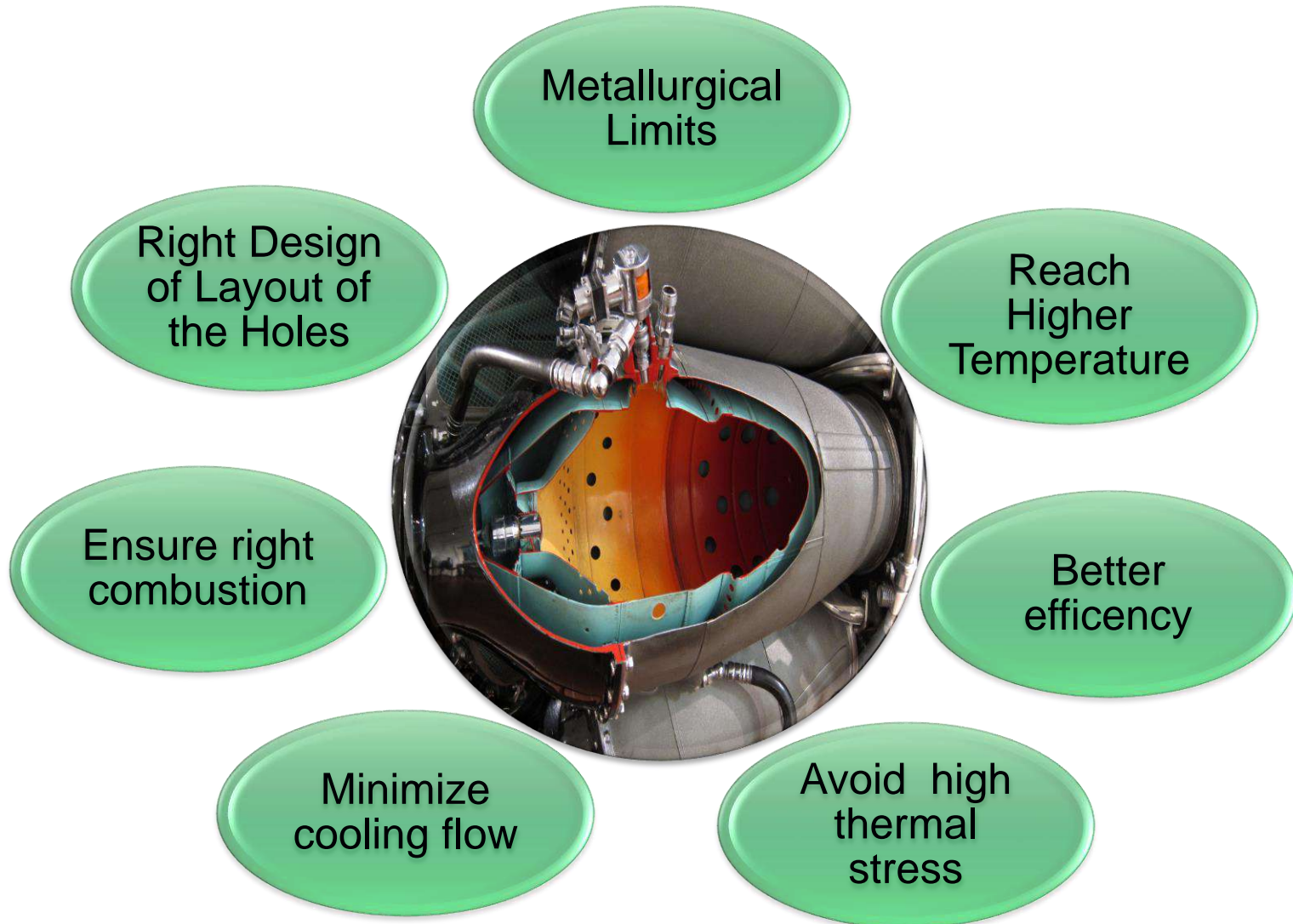
Prof. G.E. Andrews (University of Leeds)

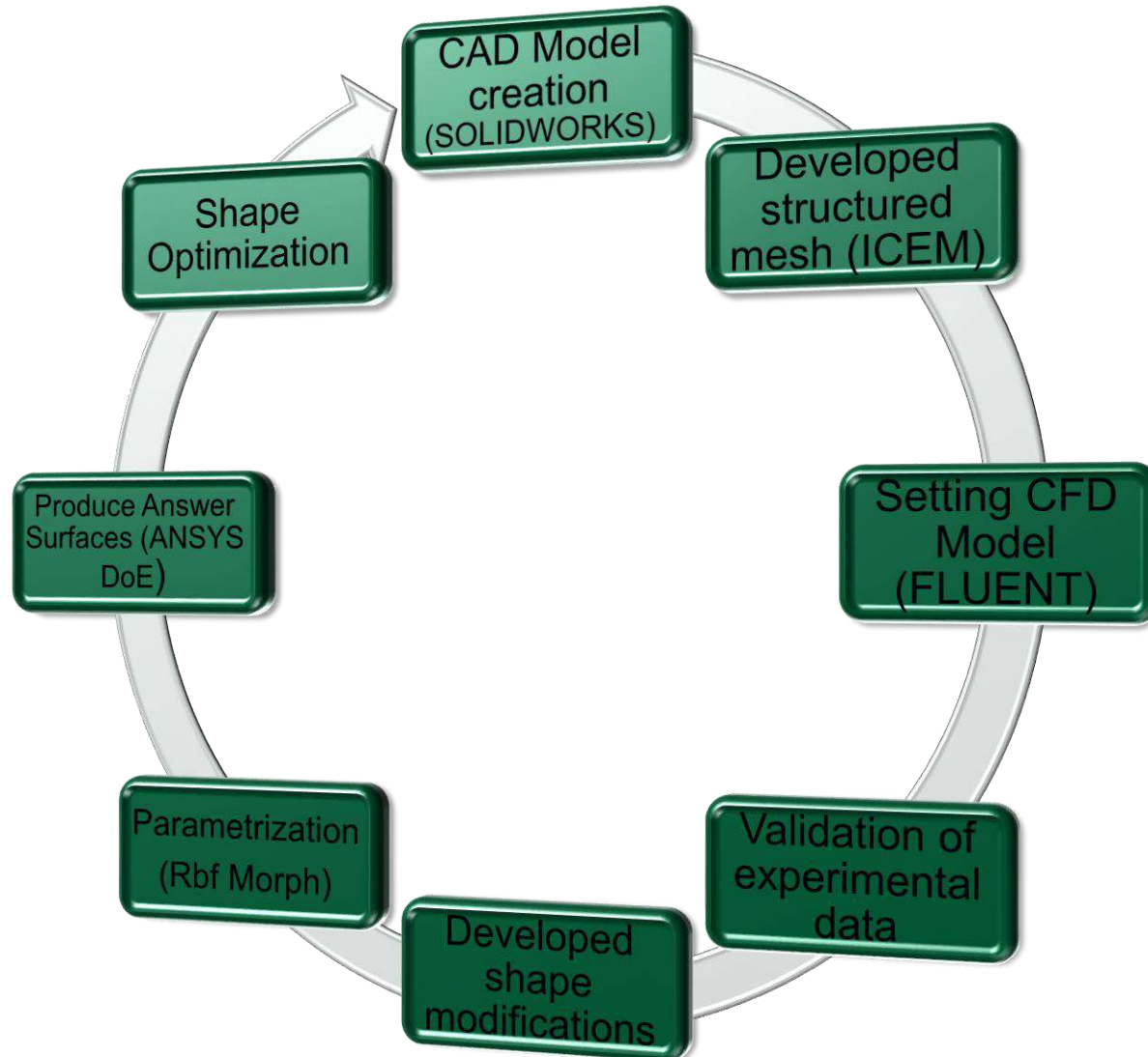
Ing. A. Pranzitelli (University of Leeds)

Laureando

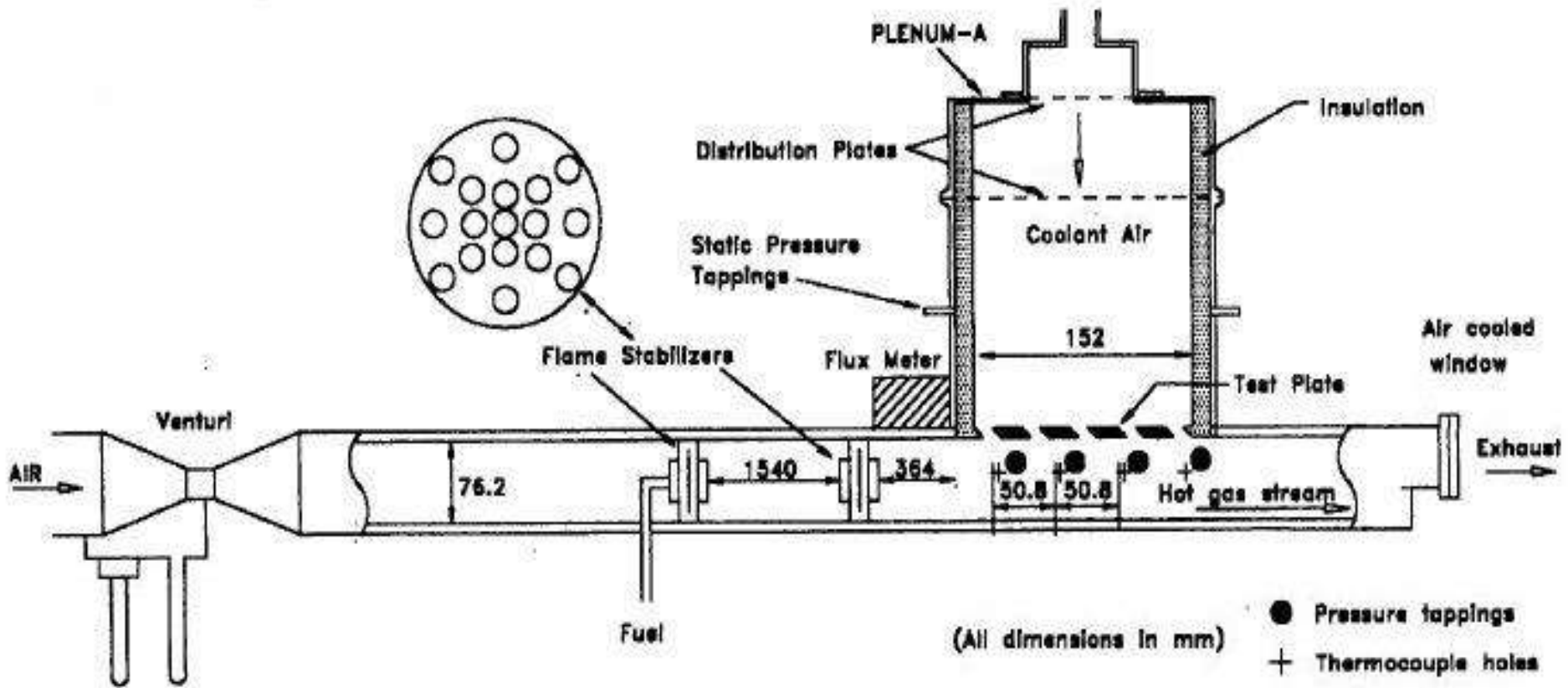
Walter Savastano

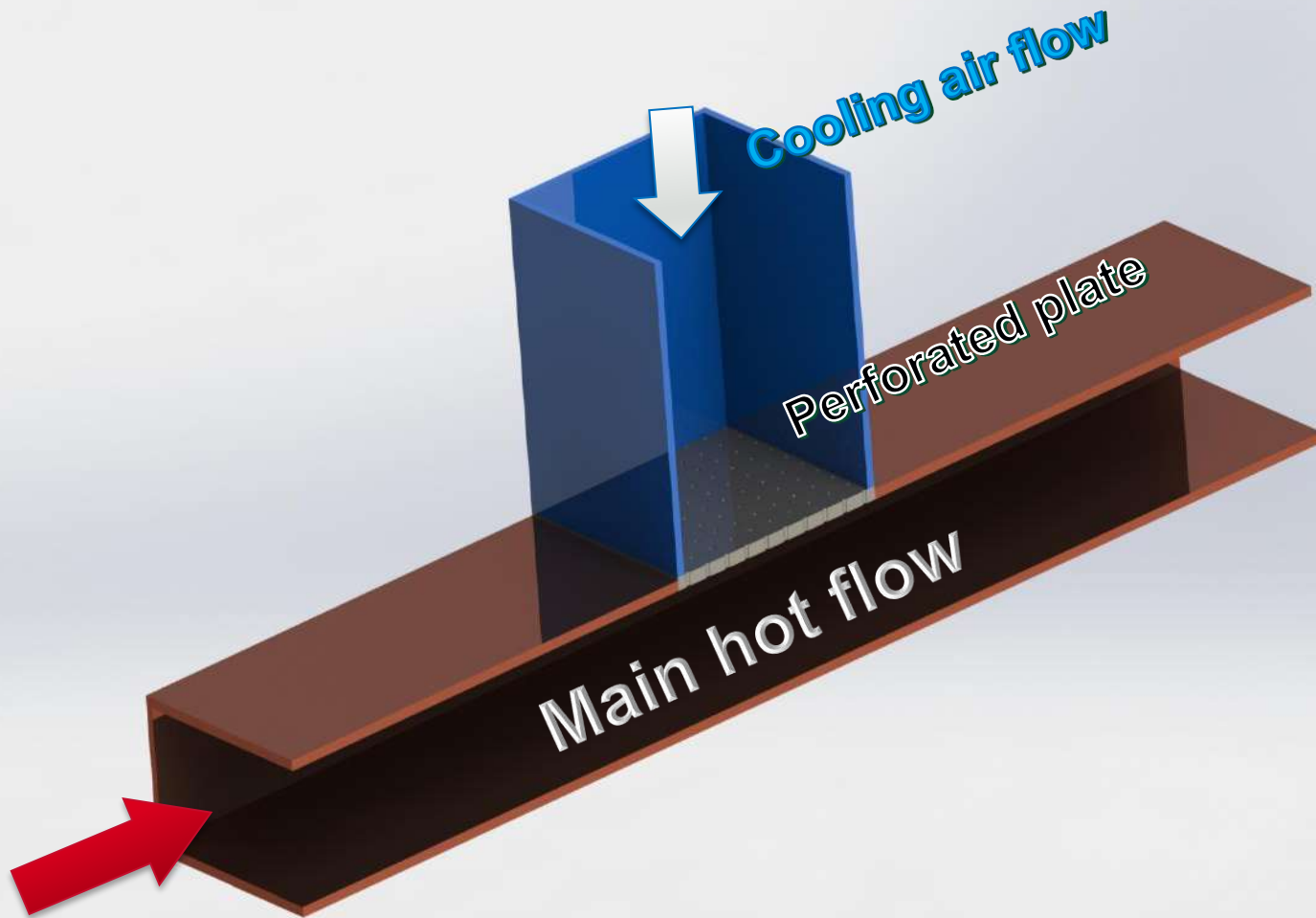
Matr. 0185986



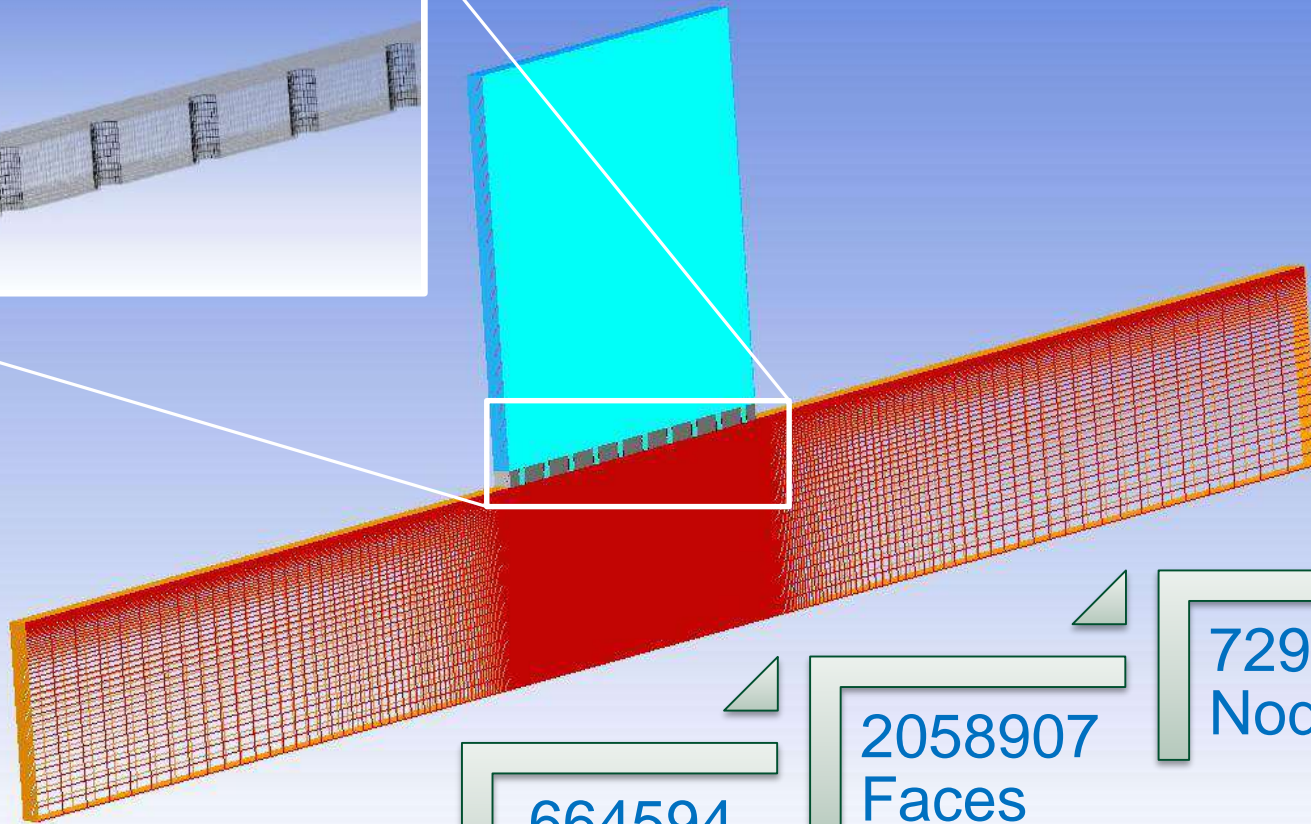
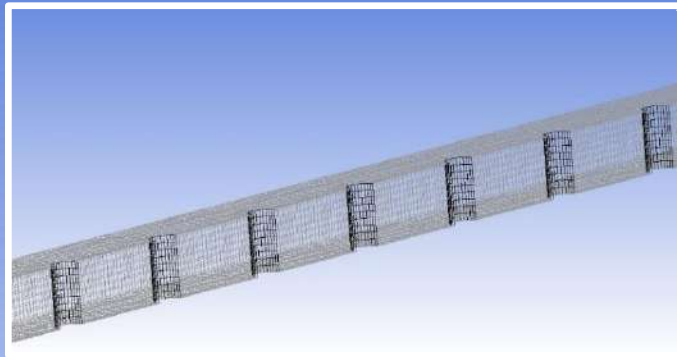


# Experimental Apparatus





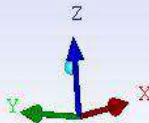
# ANSYS ICEM: Structured mesh



664594  
Cells

2058907  
Faces

729388  
Nodes



# Fluent Model

## Fluent

- Finite volume numerical calculation

## Turbulence model

- Realizable k- $\epsilon$

## Wall Function

- Standard wall-function

## Radiation Model

- Discrete Ordinate

Vel = 27 m/s

Temp = 770 K

Velocity inlet

Cold mass flow inlet

Mass flow rate  
 $G = 0.4 \text{ kg/m}^2\text{s}$

$T = 300 \text{ K}$

NIMONIC  
75

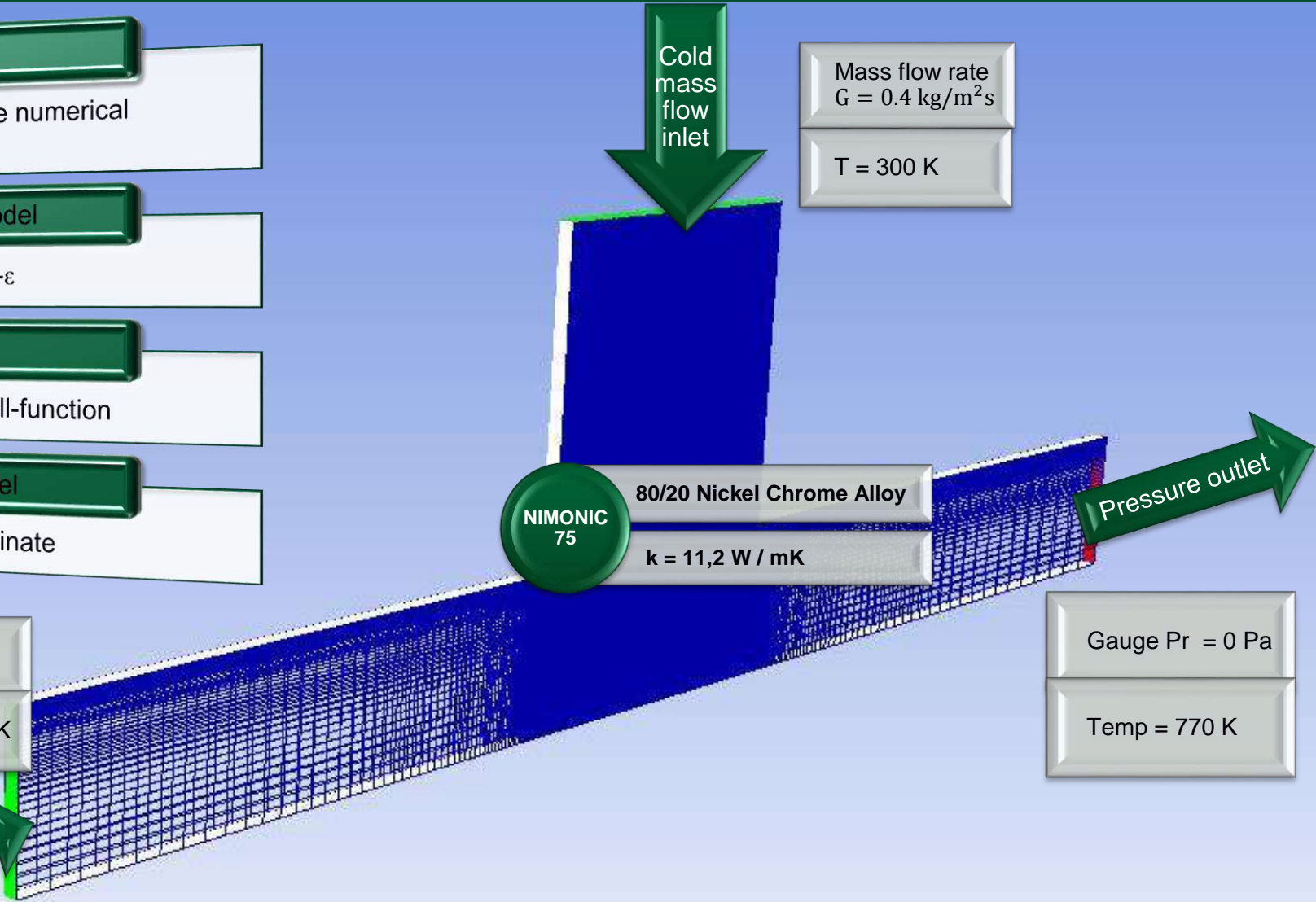
80/20 Nickel Chrome Alloy

$k = 11,2 \text{ W / mK}$

Pressure outlet

Gauge Pr = 0 Pa

Temp = 770 K



# Validation: Mesh Sensibility



Overall effectiveness

$$\eta_{ov} = \frac{T_g - T_w}{T_g - T_c}$$

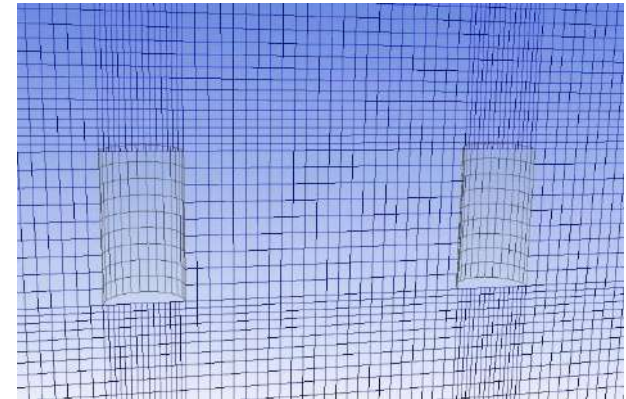
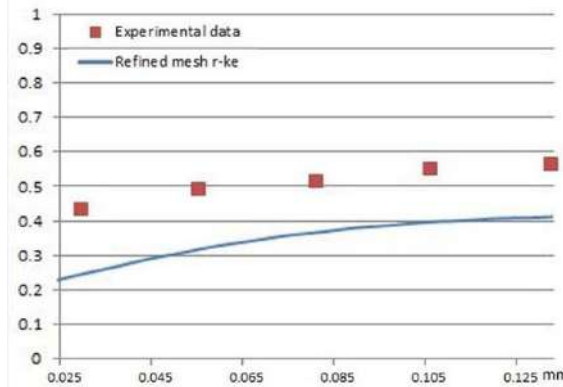
$T_g$  = Hot gas Temperature

$T_w$  = Wall temperature

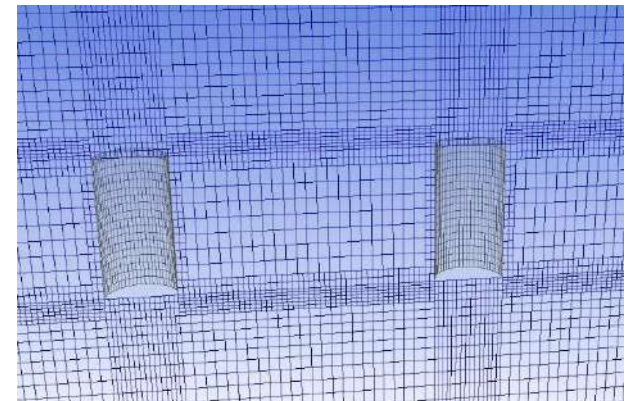
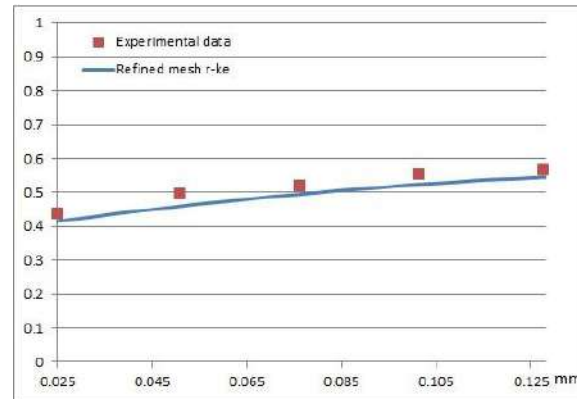
$T_c$  = Cooling air Temperature



Coarse Mesh  
(700k cells)



Refined Mesh  
(1mln cells)

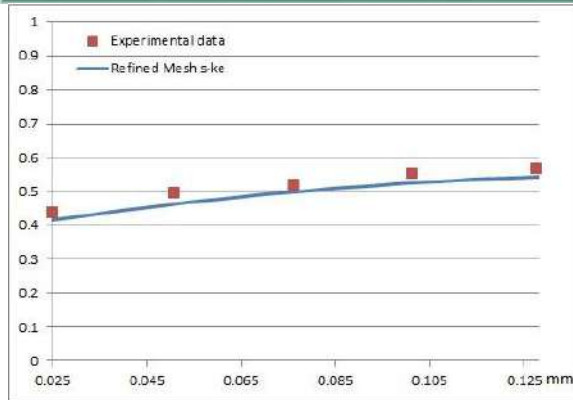




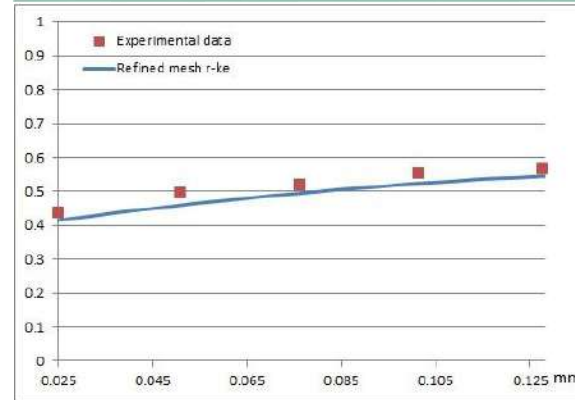
# Turbulence Model Sensibility



## Standard k-e



## Realizable k-e



Overall effectiveness

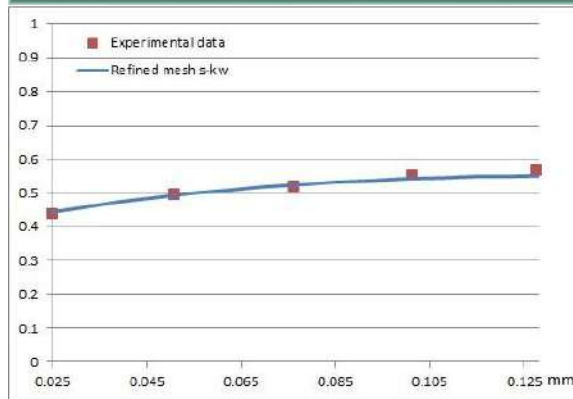
$$\eta_{ov} = \frac{T_g - T_w}{T_g - T_c}$$

$T_g$  = Hot gas Temperature

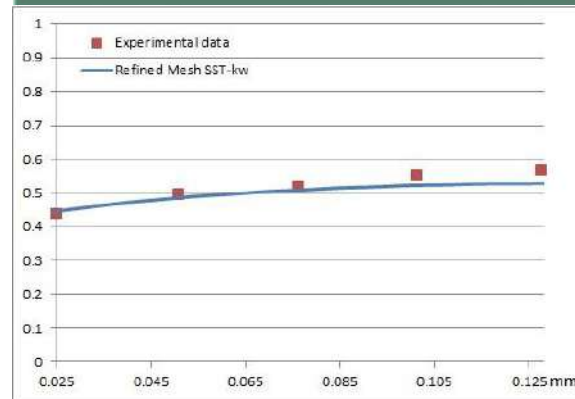
$T_w$  = Wall temperature

$T_c$  = Cooling air Temperature

## Standard k-w



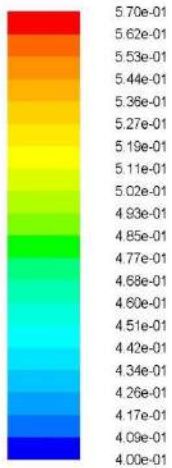
## SST k-w



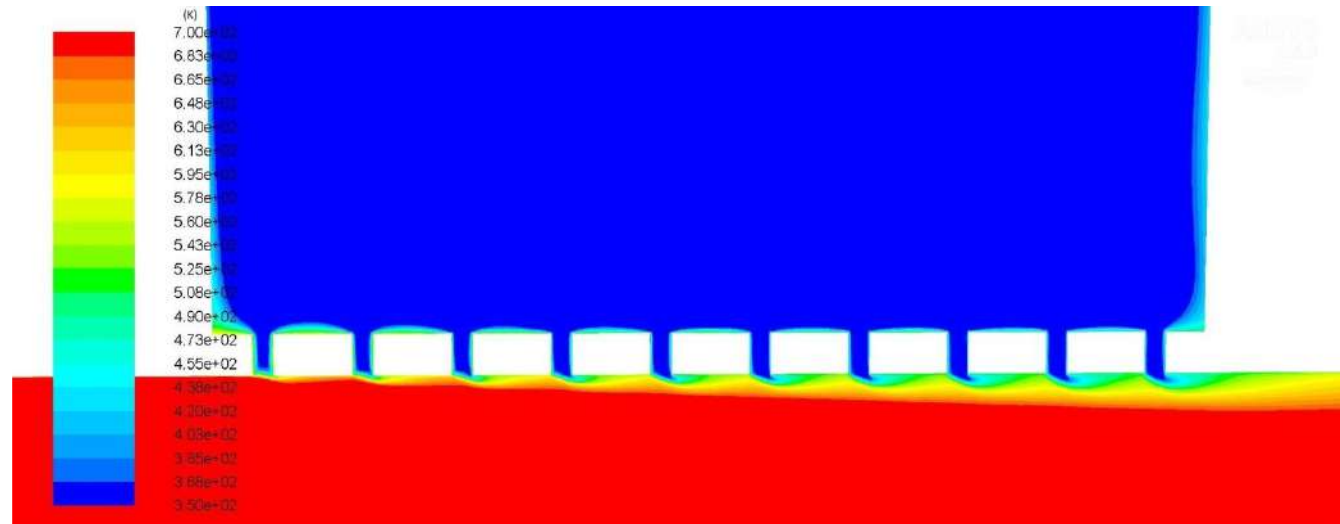
# Baseline results

*Overall Effectiveness:  
Contour on the plate*

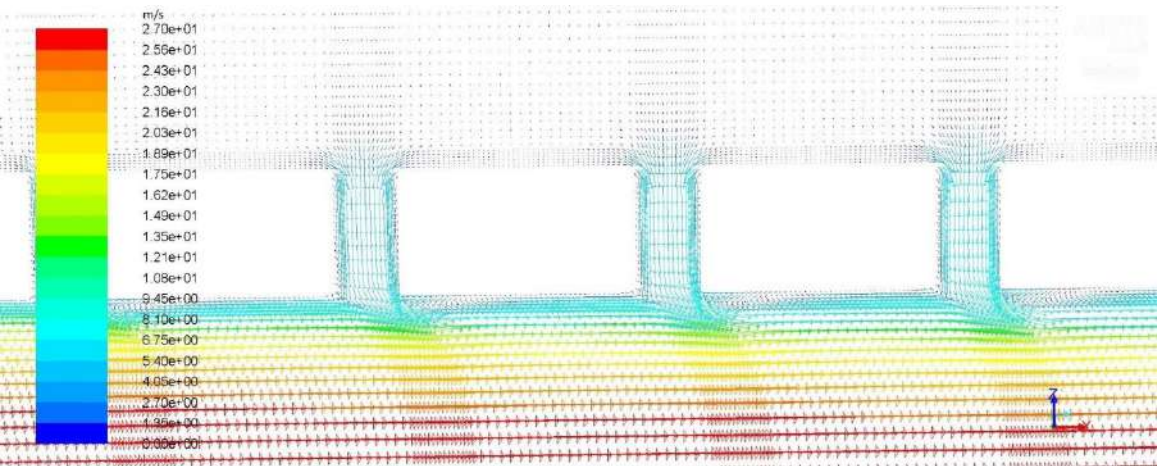
$$\eta_{ov} = \frac{T_g - T_w}{T_g - T_c}$$



*Temperature profile  
on symmetry plane*



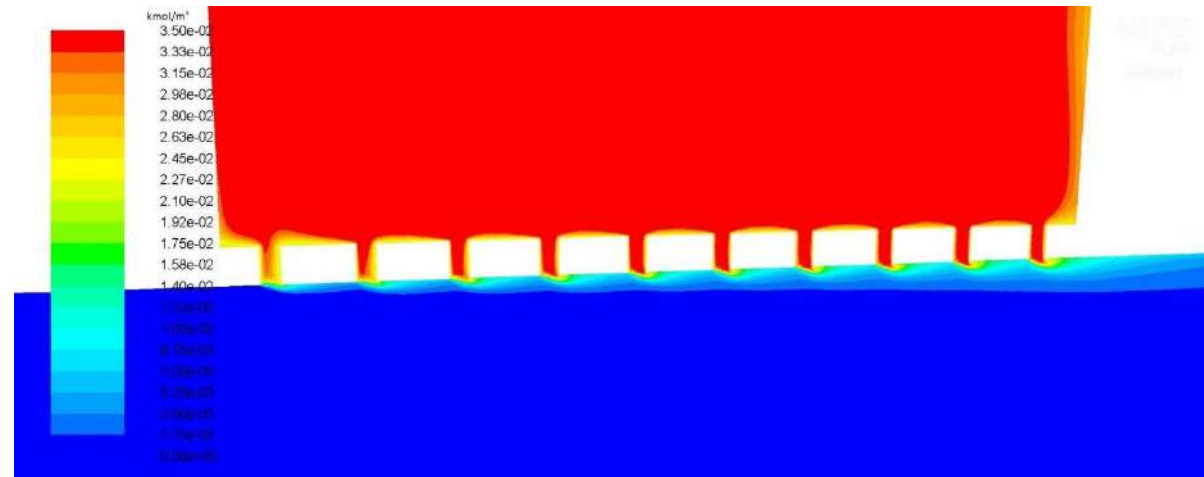
## Velocity vectors on symmetry plate

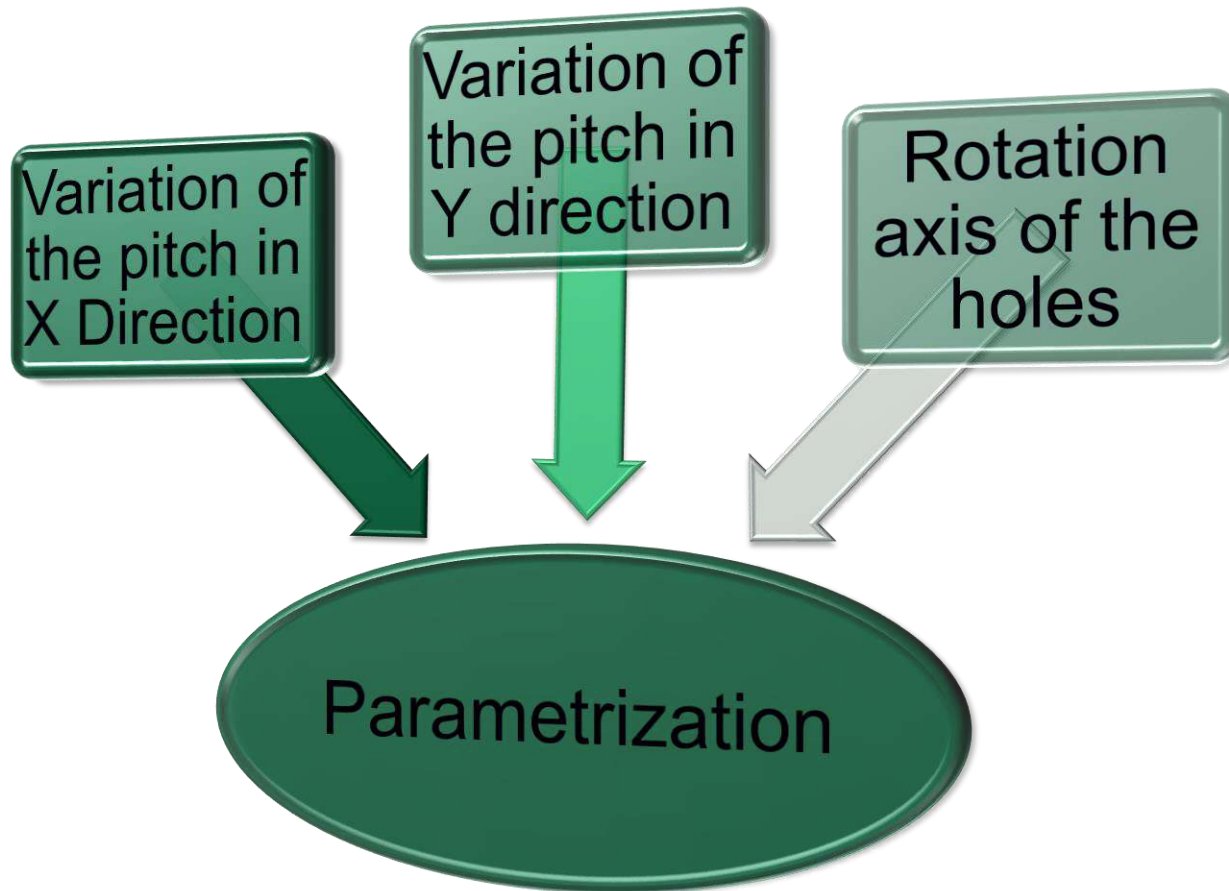


Flow separation at the exit of the holes

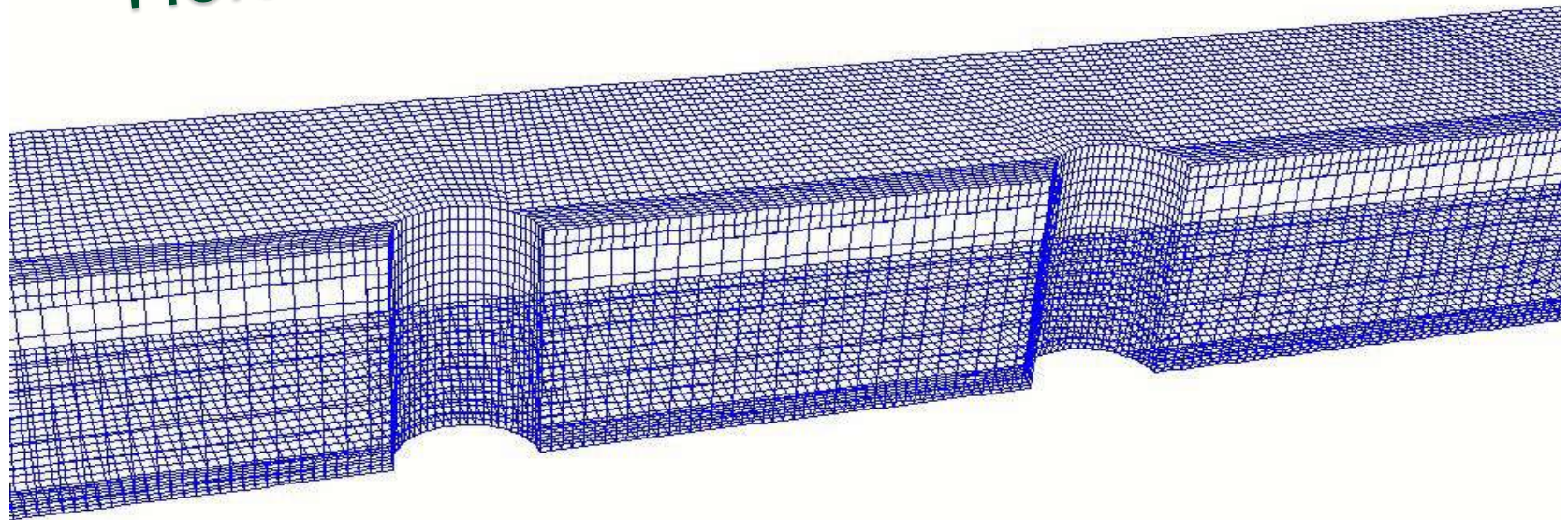
Tracer concentration on symmetry plane

*No mix between the flows*





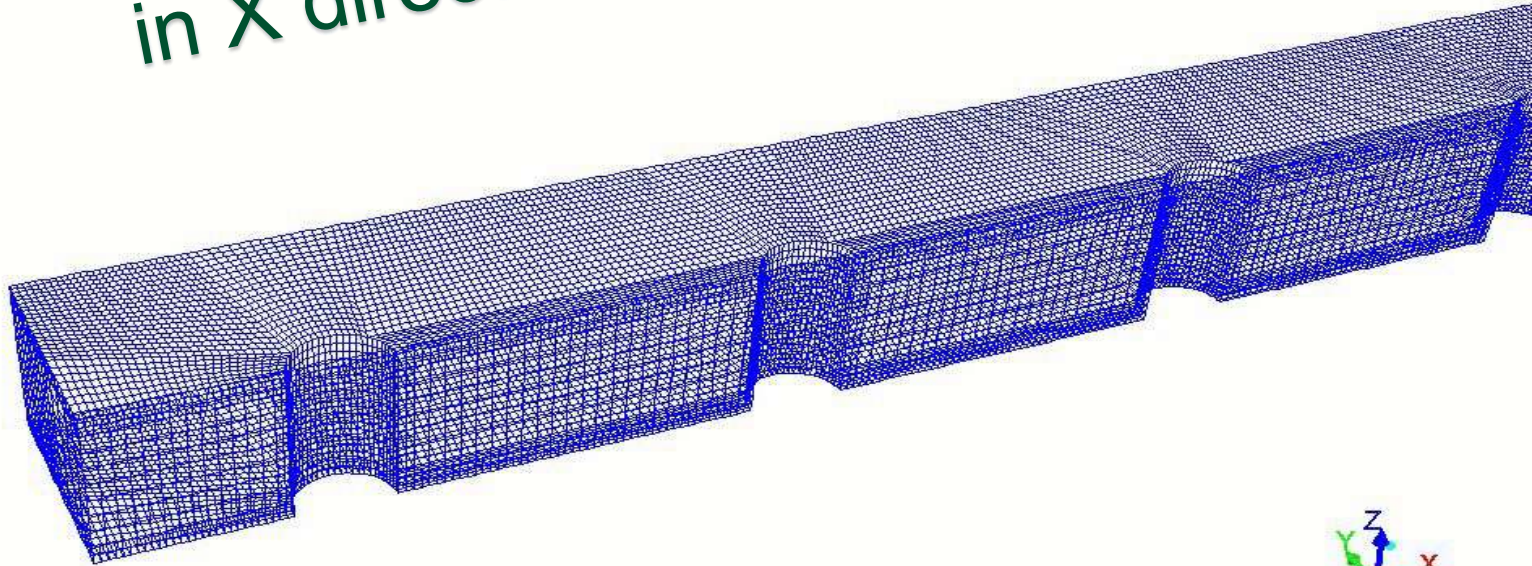
## Holes' Axis rotation



# RBF Morph Parametrization



Variation of the pitch  
in X direction

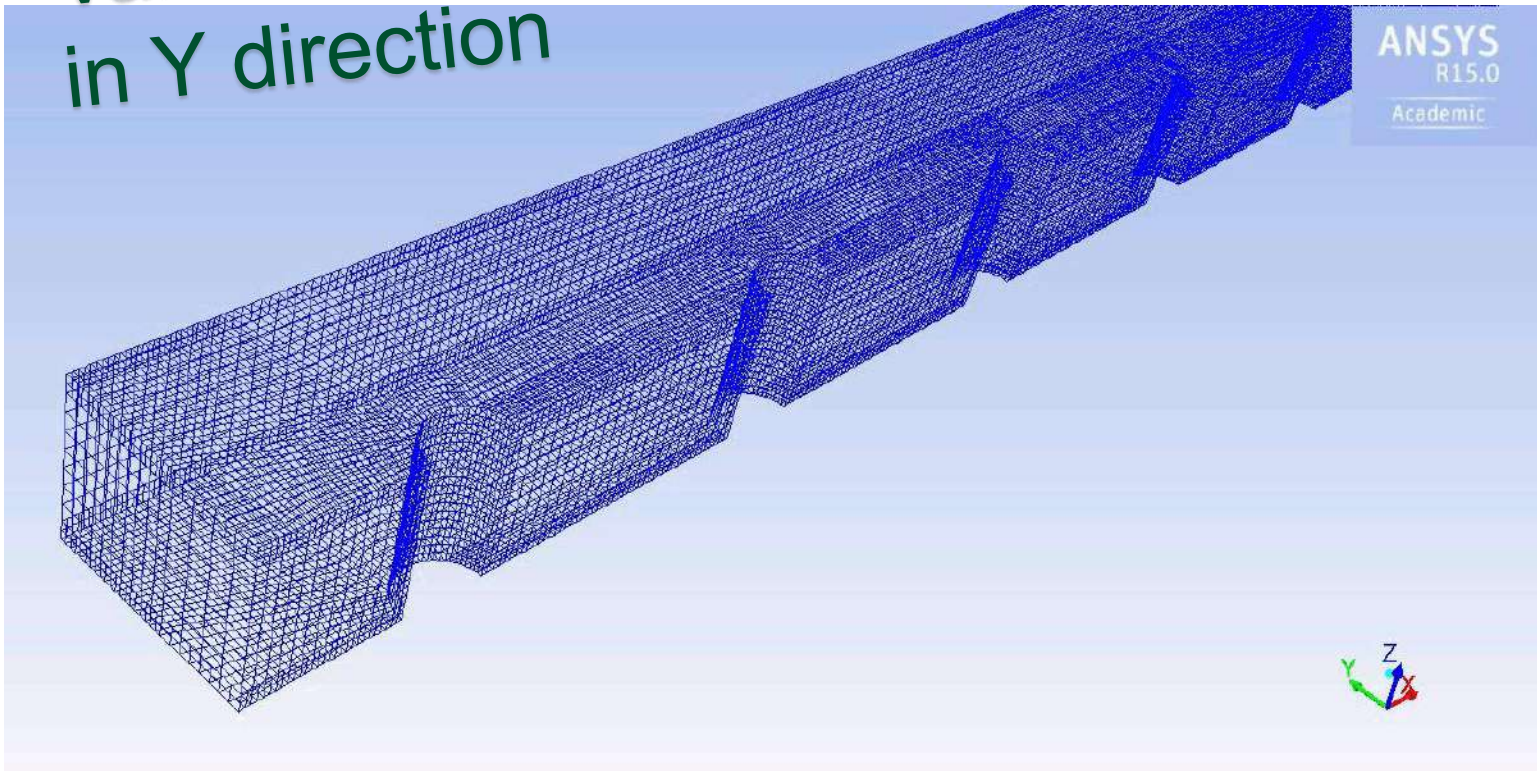


ANSYS  
RBF  
MORPH

# RBF Morph Parametrization



Variation of the pitch  
in Y direction



## Input

- Rotation
- Pitch in X
- Pitch in Y

## Output $\left( \frac{T_g - T_w}{T_g - T_c} \right)$

- **Overall effectiveness Average**
- Overall effectiveness Min **>0,4**
- Overall effectiveness Max
- Adiab. effectiveness Average (at 0,2 mm from the plate)
- Adiab. Effectiveness Max (at 0,2 mm from the plate)



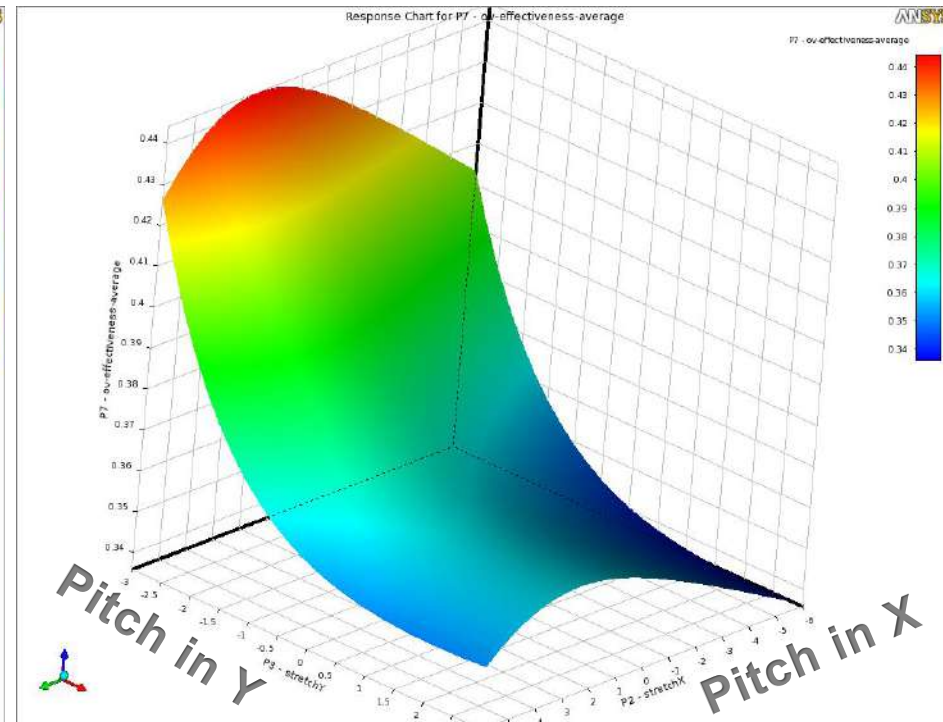
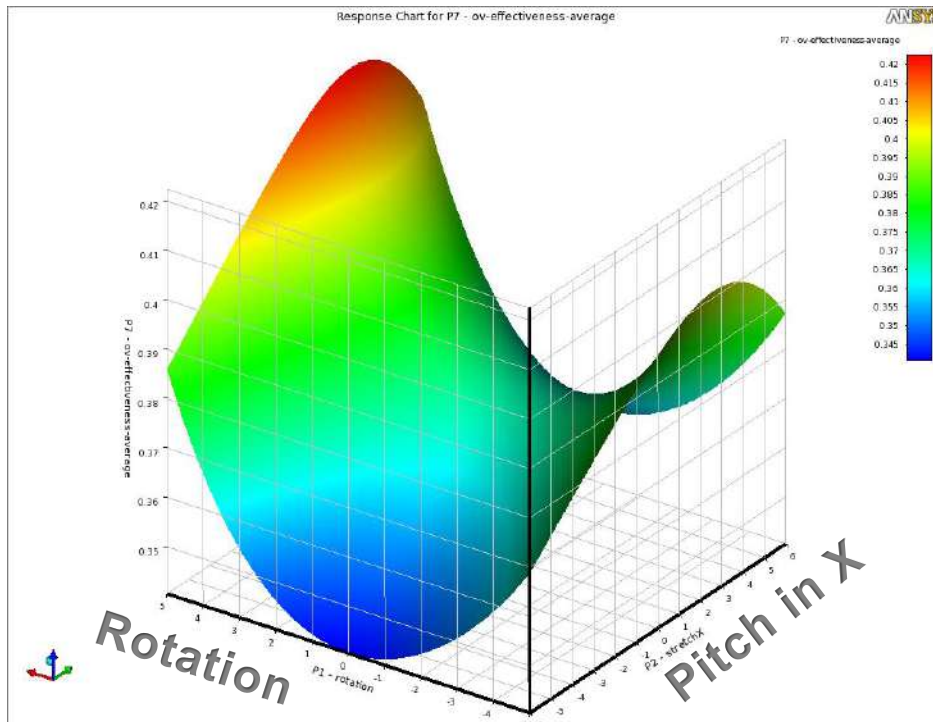
## Input

## Output

Injection angle (deg)	Pitch in x (mm)	Pitch in Y (mm)	Overall Effectiveness Min	Overall Effectiveness Average	Overall Effectiveness max	Adiabatic Effectiveness Average	Adiabatic Effectiveness Max
43°	18.8	19.5	0.408	0.468	0.616	0.243	0.356
90°	23.7	15.2	0.358	0.409	0.514	0.216	0.29
-51°	15.2	12.8	0.367	0.383	0.550	0.223	0.314
-43°	6.7	13.4	0.405	0.413	0.650	0.249	0.388
-78°	22.5	16.4	0.275	0.351	0.573	0.204	0.323
57°	10.3	18.8	0.369	0.416	0.548	0.220	0.310
-57°	21.3	11.6	0.284	0.351	0.557	0.210	0.319
-66°	17.6	17.6	0.424	0.445	0.643	0.258	0.382
-39°	7.9	17.0	0.381	0.389	0.576	0.228	0.319
51°	9.1	15.8	0.279	0.360	0.546	0.209	0.308
-35°	12.8	14.0	0.285	0.366	0.654	0.213	0.354
35°	11.6	10.9	0.338	0.407	0.596	0.242	0.342
66°	16.4	18.2	0.327	0.411	0.640	0.245	0.382
39°	14.0	14.6	0.393	0.480	0.563	0.232	0.315
78°	18.8	19.5	0.344	0.363	0.557	0.220	0.332

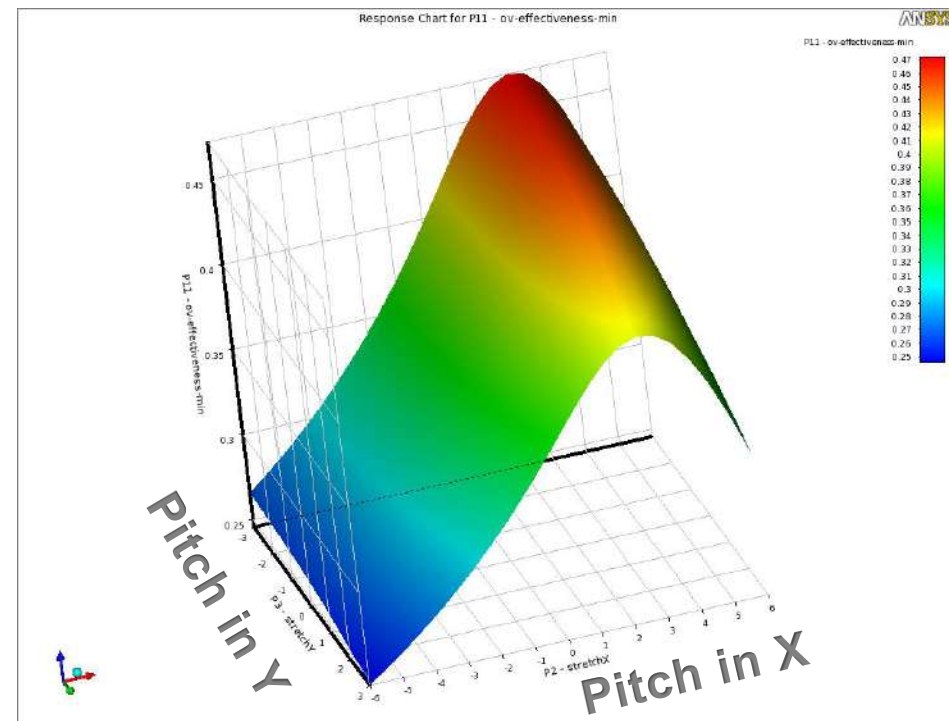
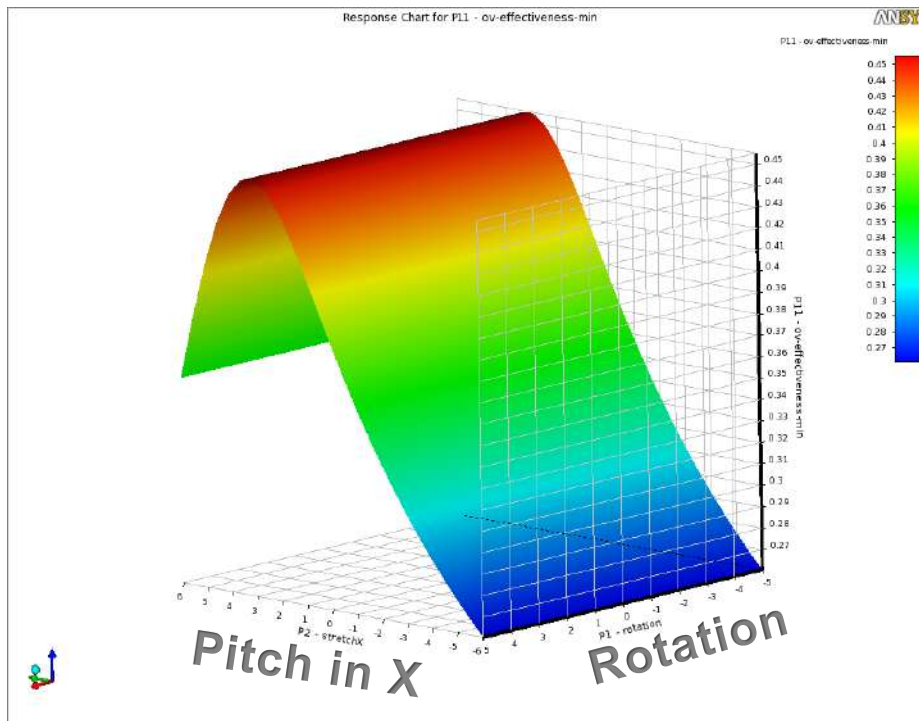
# Answer surfaces

Optimization parameter  
Overall effectiveness average =  $f(\text{Input1}, \text{Input2})$



# Answer surfaces

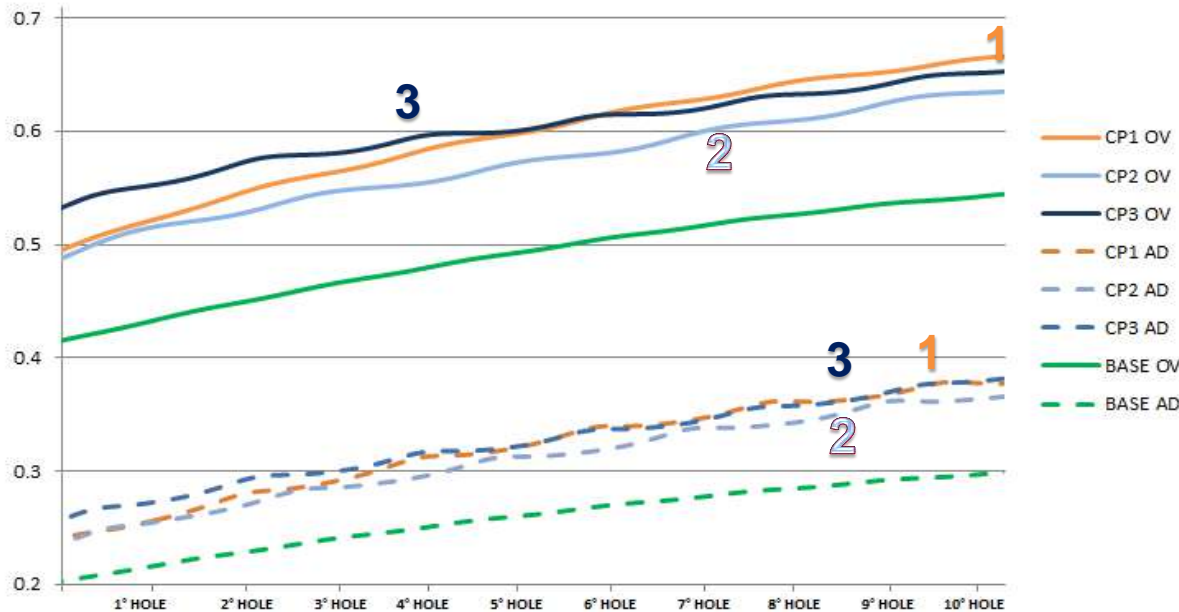
Constraint parameter  $> 0,4$   
Overall effectiveness min =  $f(\text{Input1}, \text{Input2})$



# Optimization Candidate Points



N°	Injection Angle (deg)	Pitch in x (mm)	Pirch in Y (mm)	Overall Effectiveness Min	Overall Effectiveness Average	Overall Effectiveness Max	Adiabatic Effectiveness Average	Adiabatic Effectiveness Max
BASE	90°	15,24	15,24	0.411	0.453	0.540	0.216	0.309
1	-32,7°	17,03	12,92	0.483	0.591	0.681	0.316	0.392
2	-33,2°	18,31	12,90	0.482	0.563	0.652	0.304	0.383
3	-74,6	16,72	12,90	0.524	0.603	0.668	0.338	0.403



- Improvement of 30% in overall effectiveness
- Improvement of 50% in adiabatic effectiveness
- Candidate Point N°3 :
  - Overall Effectiveness higher
  - Lower Temperature gradient along the plate
  - Ad Effectiveness higher

## Overall effectiveness on the Plate

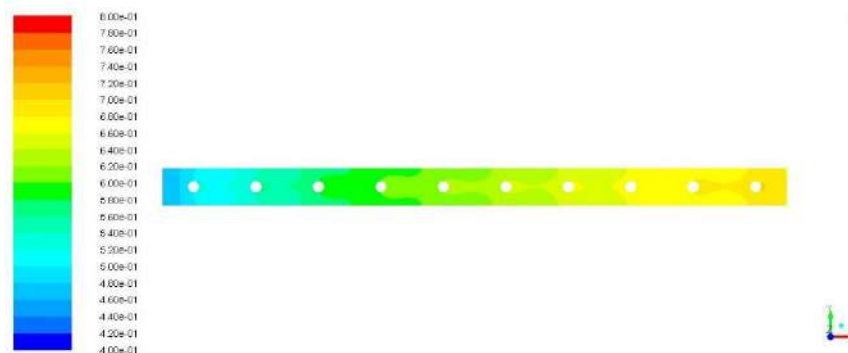
### Candidate Point N°1



### Candidate Point N°2



### Candidate Point N°3

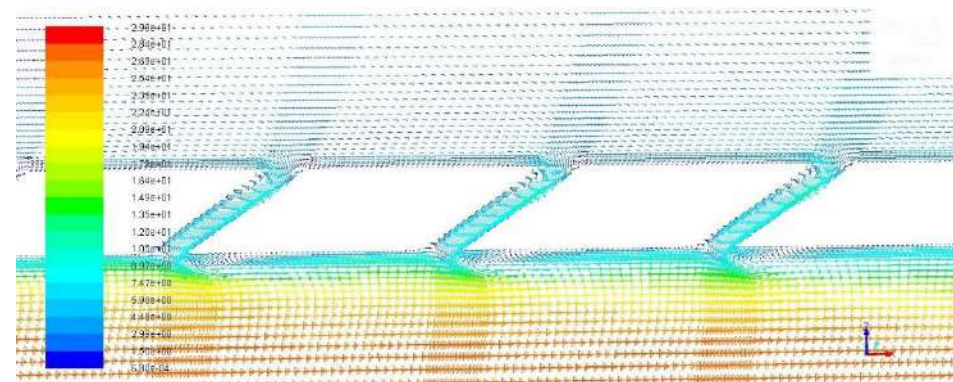
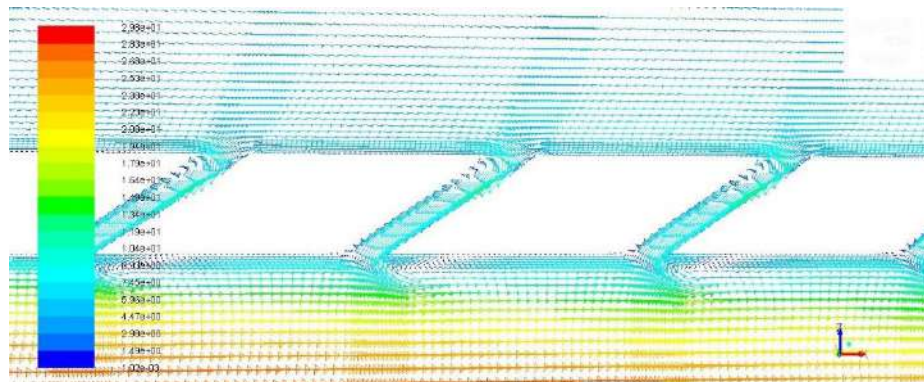


- **More homogeneous effectiveness**
- **Higher minimum effectiveness**

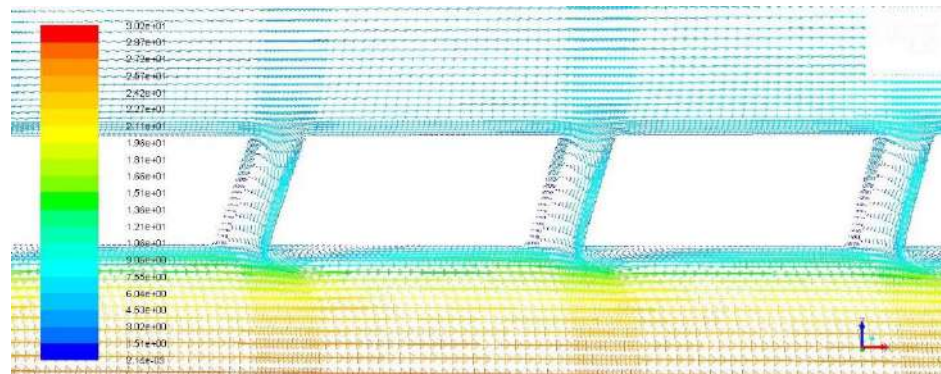
## Velocity vectors on symmetry plane

### Candidate Point N°1

### Candidate Point N°2



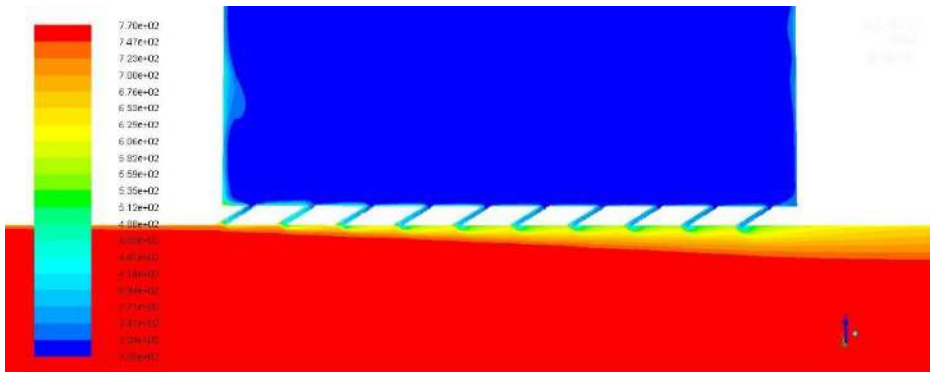
### Candidate Point N°3



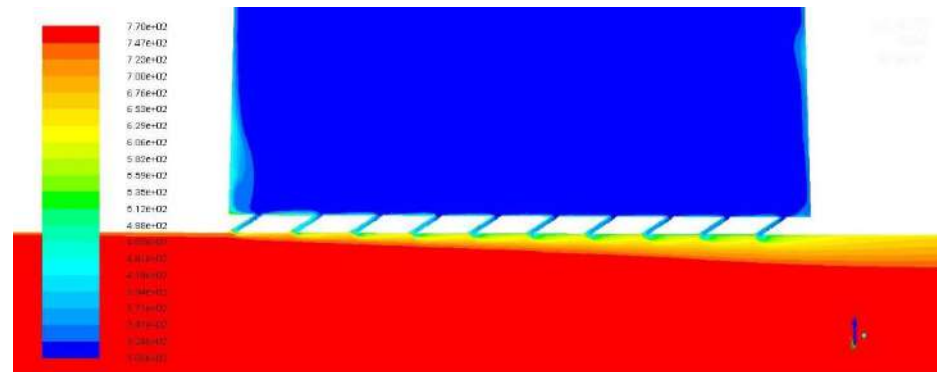
**Smaller  
detachment and  
recirculation zone**

## Temperature profile on symmetry plane

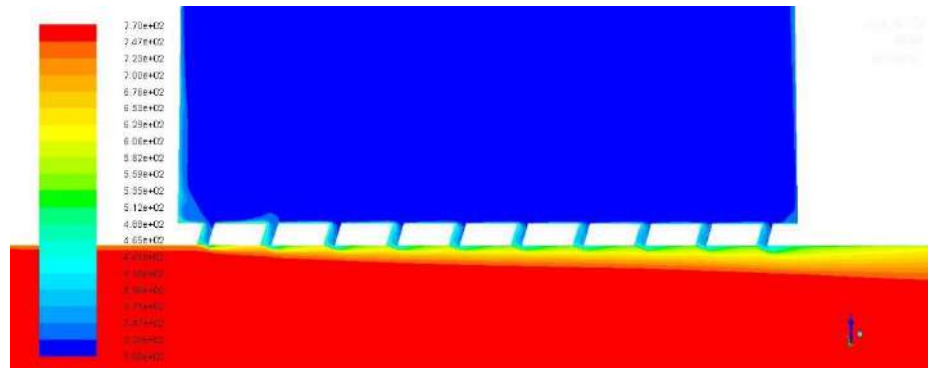
### Candidate Point N°1



### Candidate Point N°2



### Candidate Point N°3



**Better Coverage  
of the plate**

## Temperature gradient on the plate

### Candidate Point N°1

### Candidate Point N°2

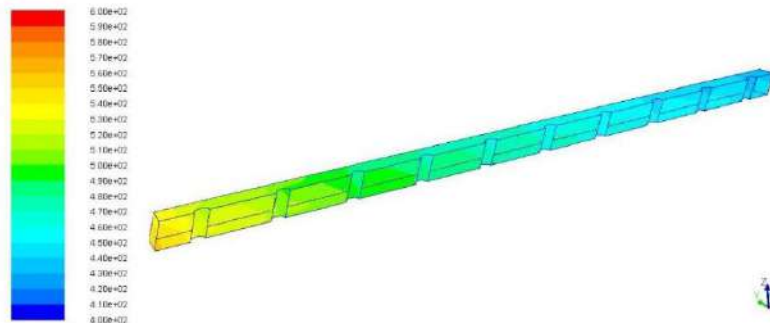
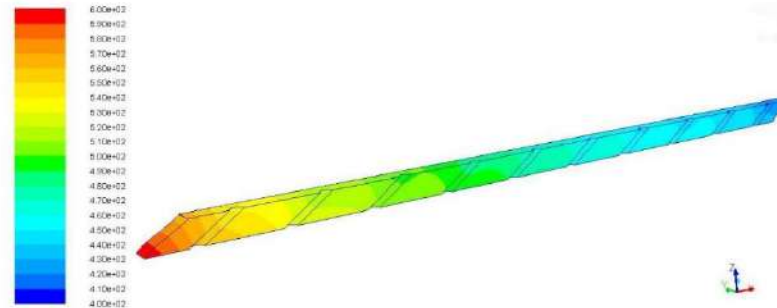
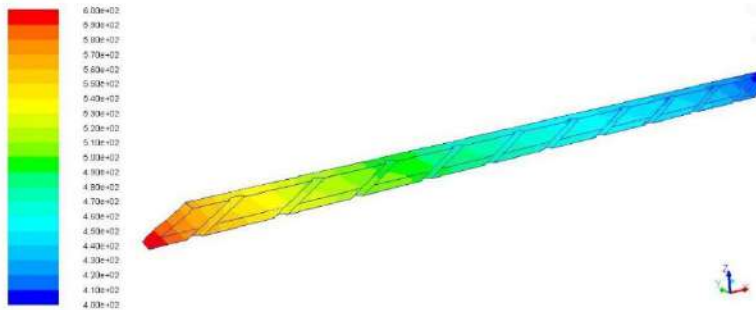
$$\nabla T_x \approx 200 \text{ K}$$

$$\nabla T_z \approx 30 \text{ K}$$

### Candidate Point N°3

$$\nabla T_x < 130 \text{ K}$$

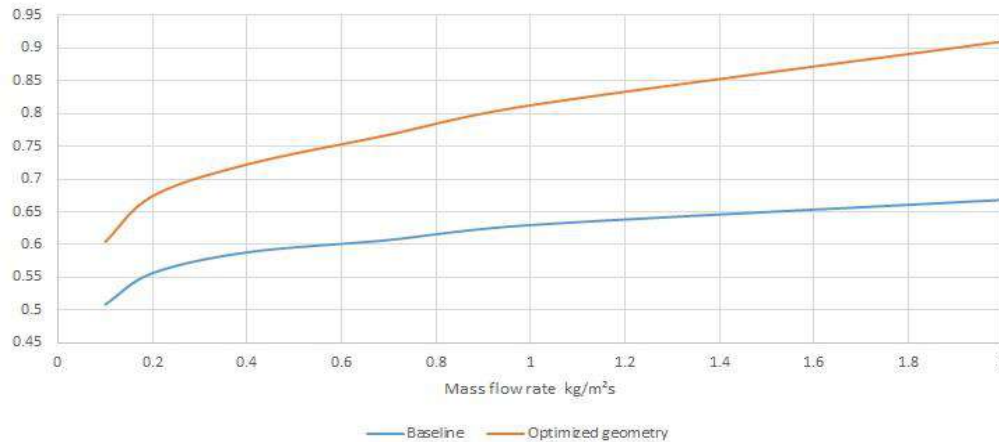
$$\nabla T_z < 10 \text{ K}$$



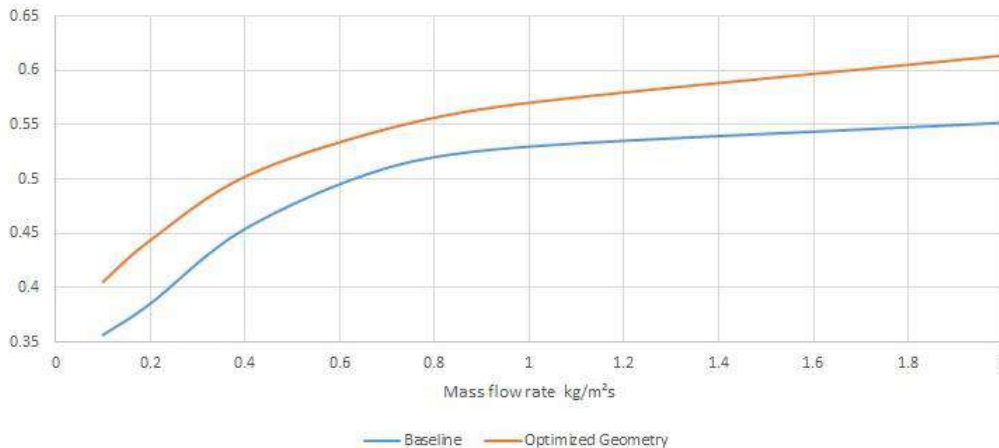


## Overall effectiveness as a function of cooling air mass flow (G)

OVERALL EFFECTIVENESS MAX



OVERALL EFFECTIVENESS MIN



- New geometry is better than baseline for all G
- Get same effectiveness with lower G
- Plateaux for high G

- CFD numerical study of an effusion cooling system developed at ***University of Leeds***
- Model validation matching experimental data obtained from:  
G E Andrews, A A Asere, M L Gupta and M C Mkpadi,  
“Effusion cooling: the influence of the number of holes”  
*Proceedings of the Institution of Mechanical Engineers, Part A: Journal of Power and Energy* 1990
- Shape optimization performed by means of Rbf Morph and Ansys Workbench suite
- Results analysis to get influence of the shape parameters on the effusion cooling effectiveness, improvement of 30%
- Found an optimal geometry reducing up to 10 times cooling air flow, without reducing effectiveness.



# MONTREAL

ASME TURBO EXPO 2015 Palais des Congrès | June 15-19



W. Savastano, A. Pranzitelli, G. E. Andrews, M. E. Biancolini, D. B. Ingham, M. Pourkashanian,

**“Goal driven shape optimisation for conjugate heat transfer in an effusion cooling plate”,**

Asme Turbo Expo, Montreal, Québec 2015



UNIVERSITY OF LEEDS

Thank you for your attention

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