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HYBRID EVENT

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UNIVERSITÀ DEGLI STUDI DI ROMA

EUROfusion

Reshaping the DEMO Tokamak's TF Coil with high fidelity Multiphysics CAE and advanced mesh morphing

Corrado groth¹, Andrea Chiappa¹, Christian
Bachmann², Francesco Maviglia², Valerio Tomarchio³,
Marco Evangelos Biancolini¹

1. University of Rome Tor Vergata - 2. EUROfusion Consortium - 3. JT-60SA European Home Team



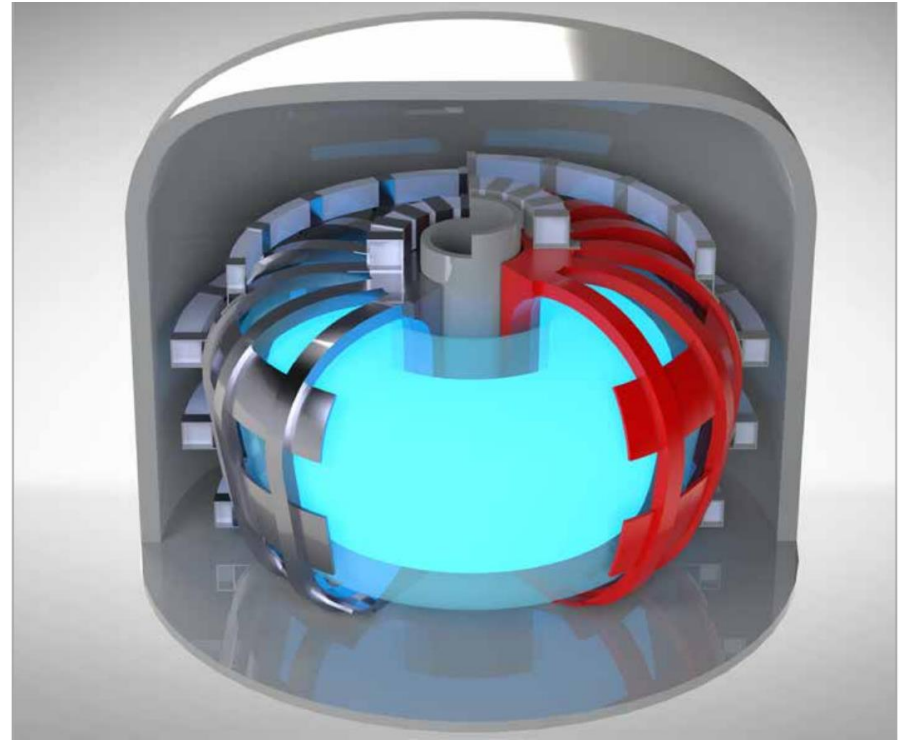
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Have a look at the 3D printed prototype showing
the effect of shape optimization



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Introduction

- A DEMONstration powerplant: the next step in EU's ambitious nuclear fusion power generation project
- DEMO will produce net electricity, design more challenging as compared to ITER: foreseen plasma power four times higher
- New technologies and concepts required. Divertor Tokamak Test (DTT) facility currently under design.

Introduction

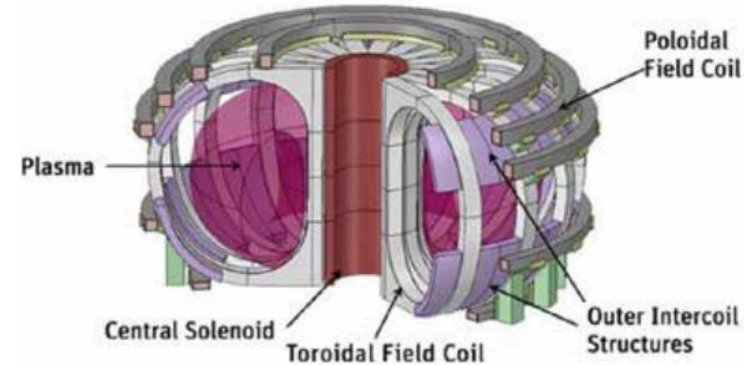
- DEMO is a challenge from a technical and technological point of view for several reasons:
 - Multiphysics involved, often leading to a trade-off of opposing requirements
 - Unprecedented range of operation for each sub-system of the assembly
- In this presentation, we show an optimization strategy for the Toroidal Field (TF) coils of the Advanced Divertor Configurations (ADCs).

Introduction

- Target: best compromise between electromagnetic and structural compliance
- Ansys simulation tools to reach the final goal:
 - **APDL** for the electromagnetic and structural analysis of the basic ADC configurations for a preliminary stress assessment
 - **Workbench + RBF Morph + APDL** to define an optimal shape (iso-stress profile) for each TF coil progressively mixing the initial and the iso-stress shape of each ADC coil to find the best compromise between the two.

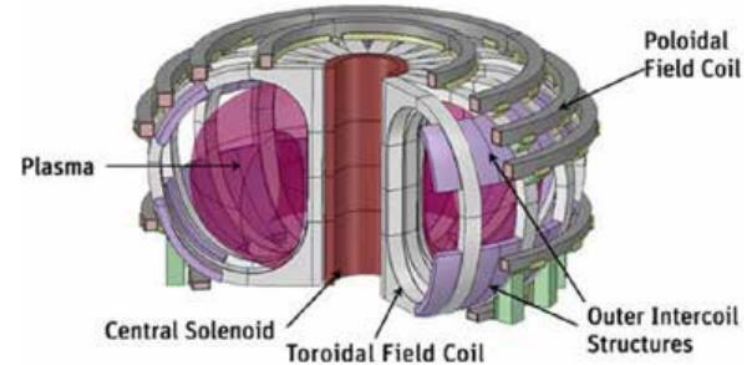
DEMO architecture

- Fusion reaction takes place inside the plasma: large amount of energy at the expense of a small portion of mass.
- Plasma is confined in a toroid chamber by magnetic fields
- Magnetic fields generated by superconductors: TF, PF, CS
- Superconductors arranged in arrays called Winding Packs (WP), cooled with supercritical helium



DEMO architecture

- Coils subject to enormous Lorenz forces
- Superconductors contained in steel casing to:
 - Shape the superconducting loops appropriately
 - Bear the impressive loads involved
- ADC designed to fulfill the first. We want to improve the latter.

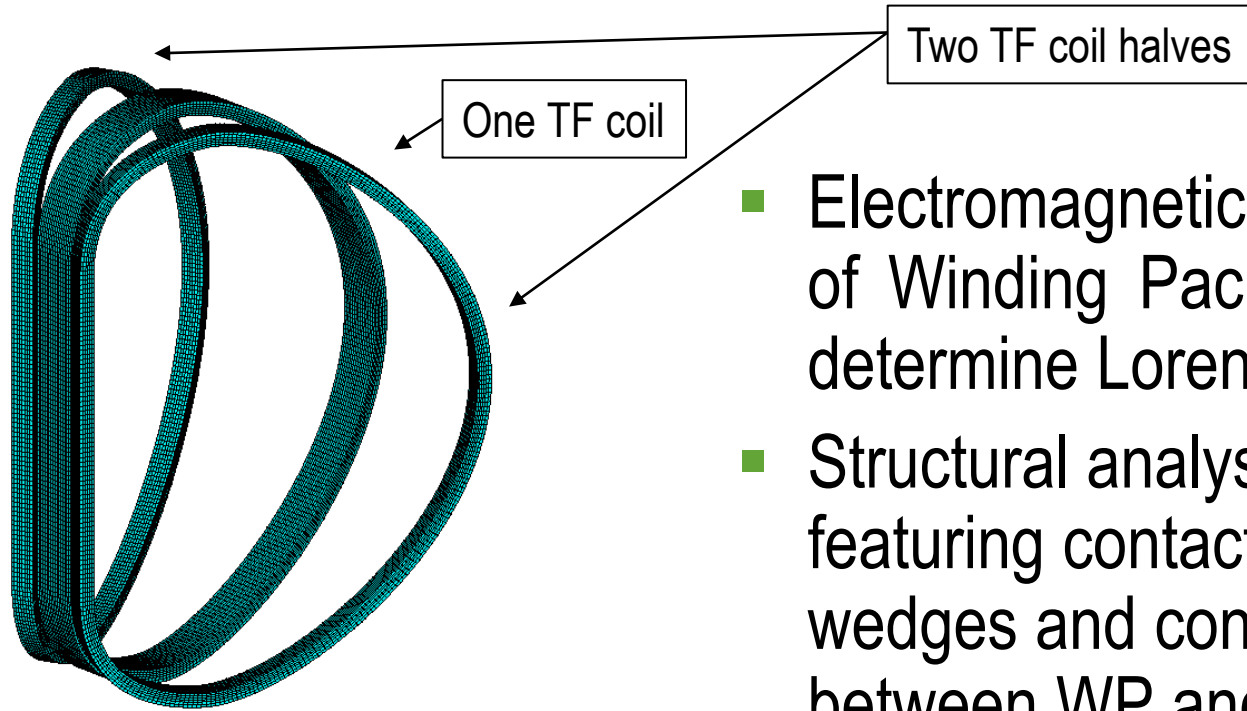


- First step:
ADC configurations used for
Electromagnetic and
structural analyses

SN, DN, SF, SX Stress results

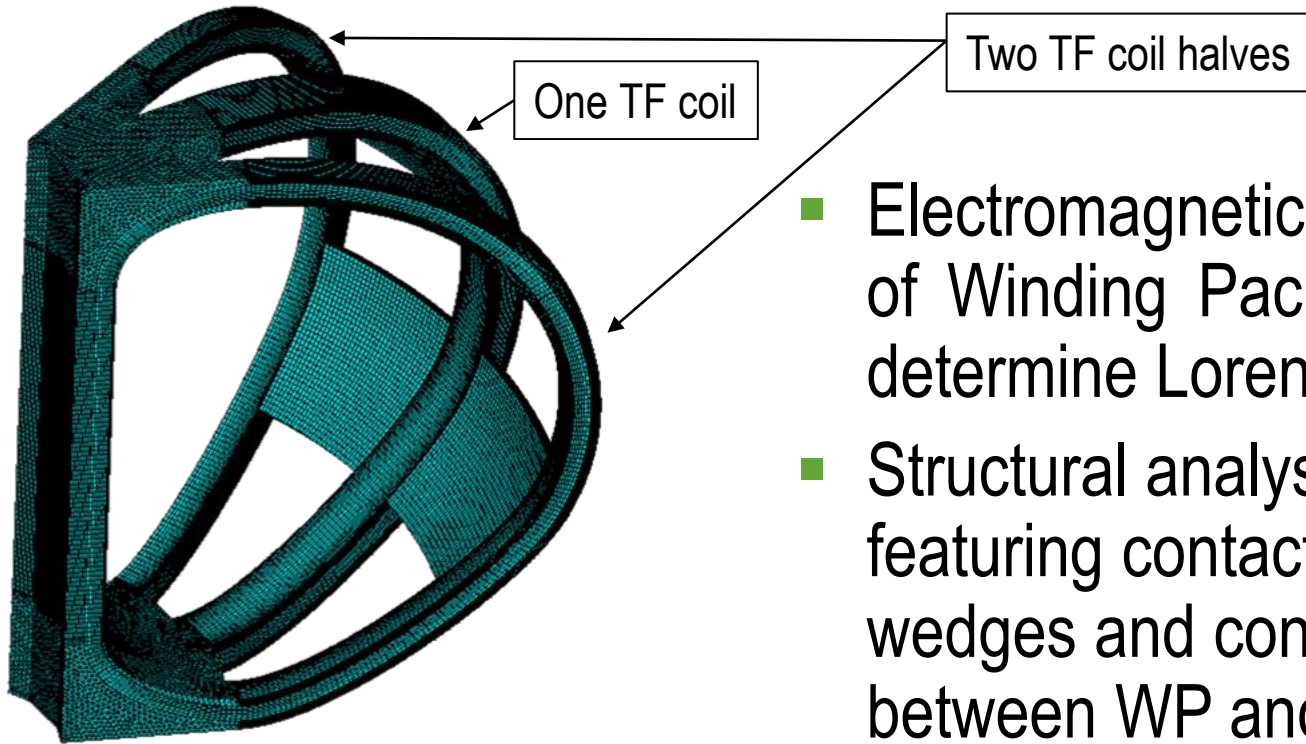
- Results were achieved on a numerical mesh counting ~ 1 Mil elements
- Basic configurations of all the ADCs studied: Single-Null (SN), Double-Null (DN), Snow-Flake (SF) and Super-X (SX)
- Electromagnetic analysis followed by structural study in APDL
- EM considering current flowing in TF coils only as happening during the magnetization stage. Lorentz forces on superconductors sent to structural analysis on same mesh

TF coil : EM model



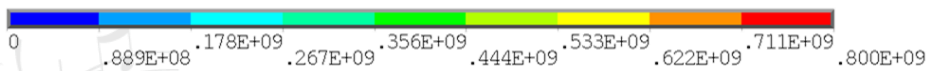
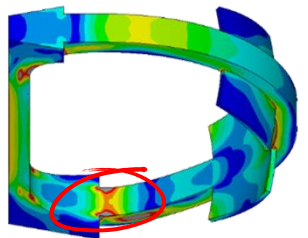
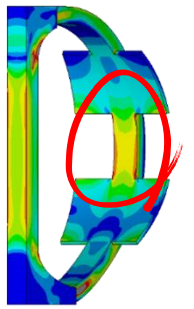
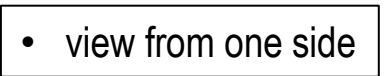
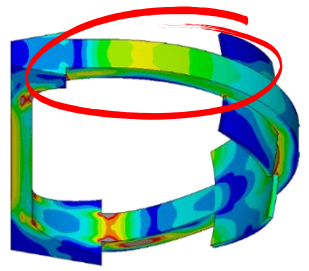
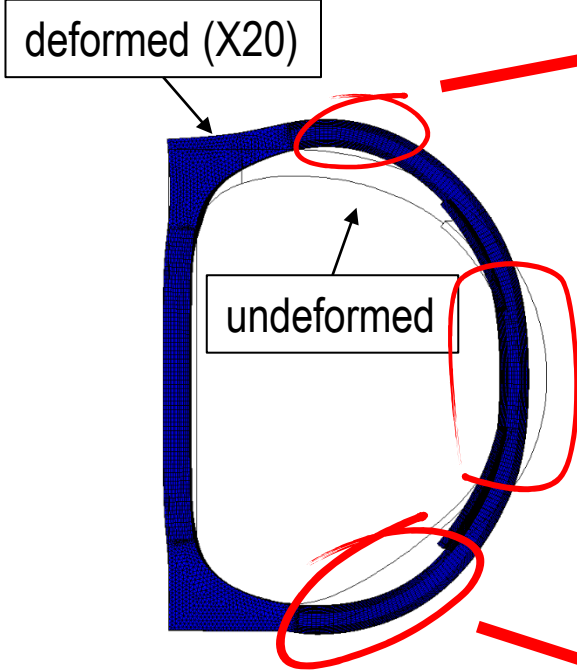
- Electromagnetic analysis of Winding Pack (WP) to determine Lorentz forces
- Structural analysis featuring contact between wedges and contact between WP and casing

TF coil : structural model

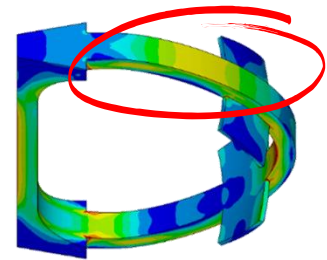
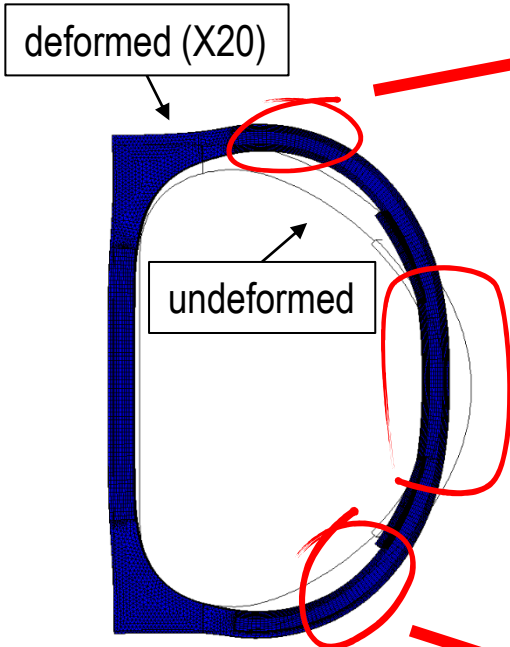
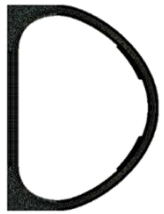


- Electromagnetic analysis of Winding Pack (WP) to determine Lorentz forces
- Structural analysis featuring contact between wedges and contact between WP and casing

SN magnetization stage

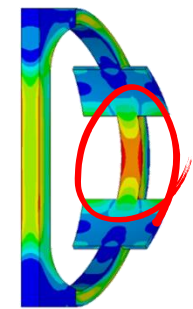


DN magnetization stage

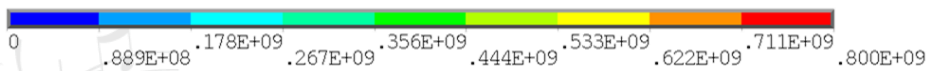
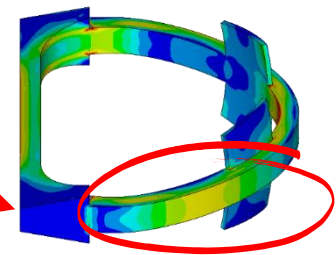


Von Mises stress:
• view from above

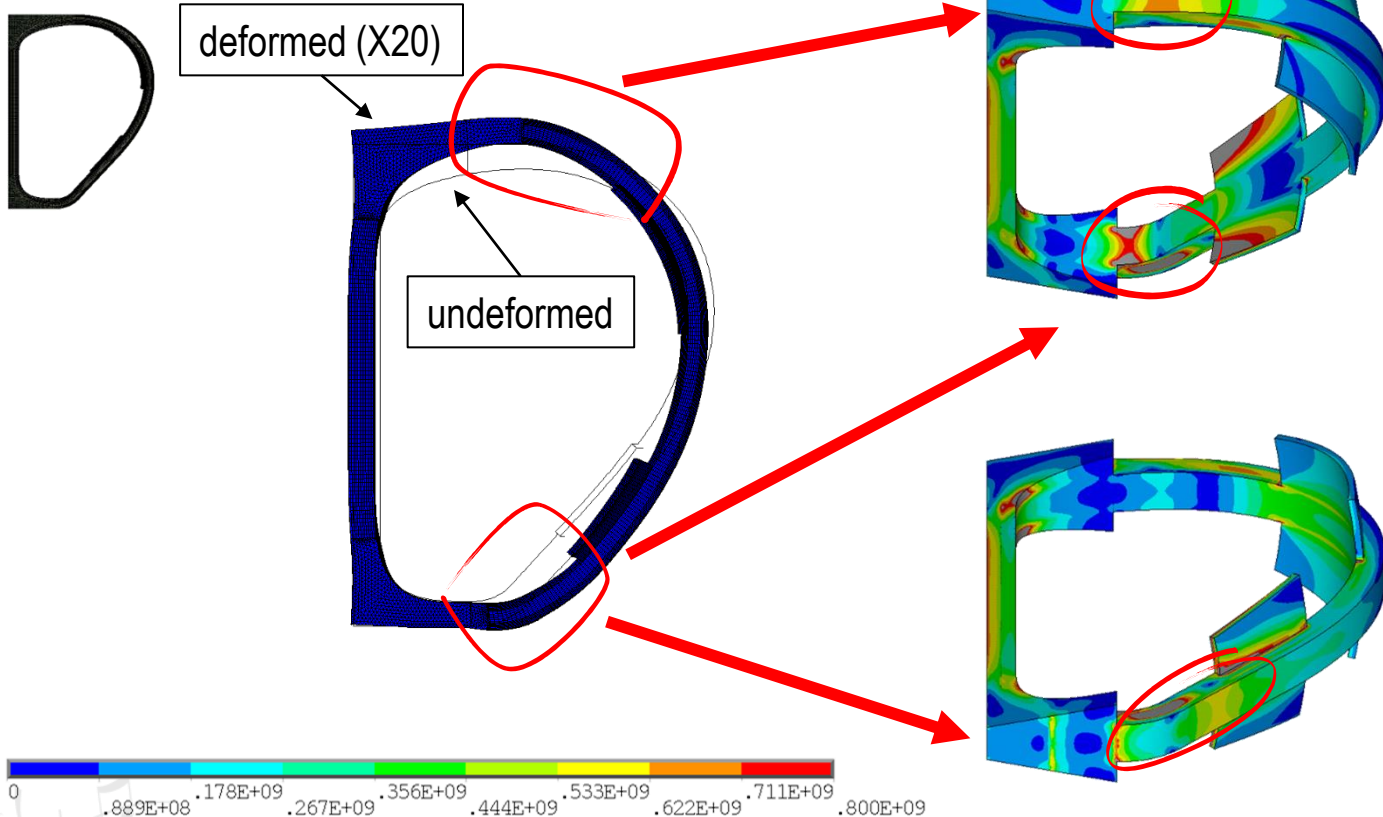
• view from one side



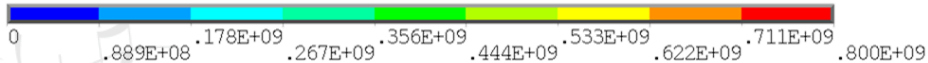
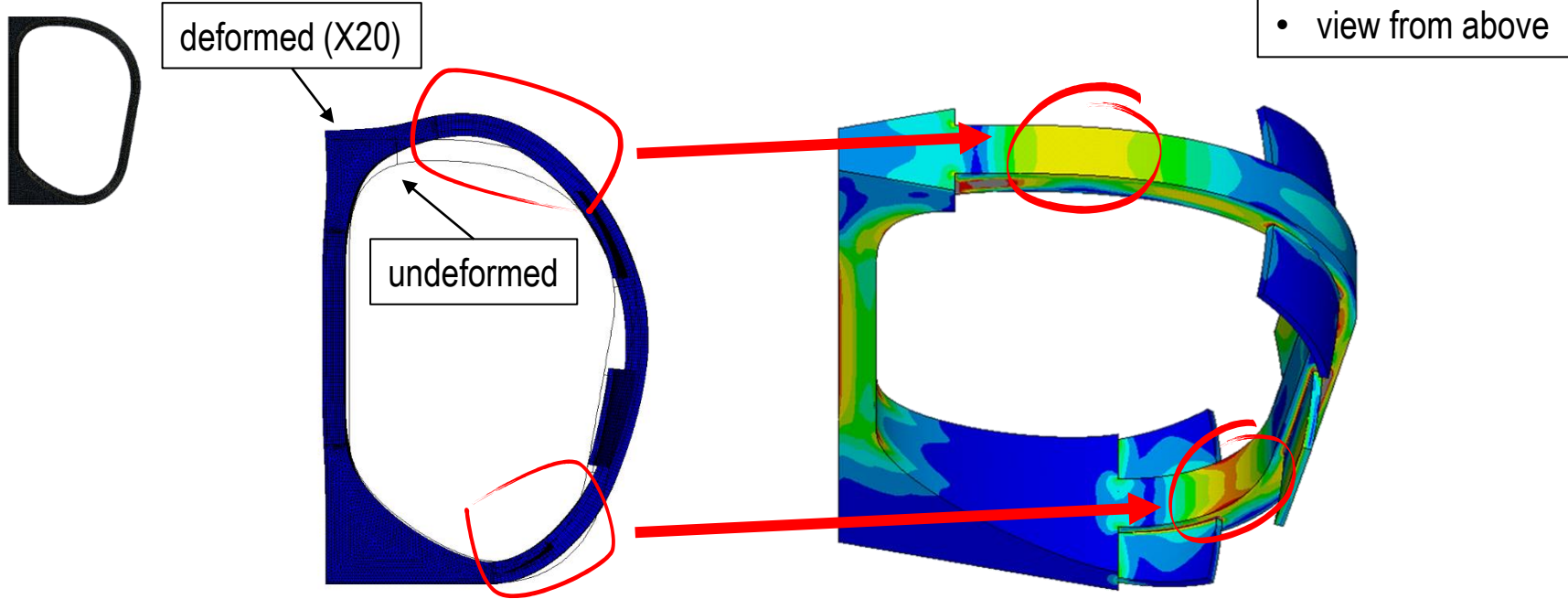
• view from below



SF magnetization stage



SX magnetization stage



ADC baseline stress results

- For each coil resultant radial force (RX) and resultant angular moments around the toroidal direction (MY):

Resultant component	SN	DN	SF	SX
RX (radial) [MN]	-860.211	-910.373	-917.155	-943.783
MY [MN•m]	341.530	0.182	9.053	1146.301

- Von Mises (VM) stresses over ADC casings reveals that large areas of material are above the assumed stress limit (700 MPa)

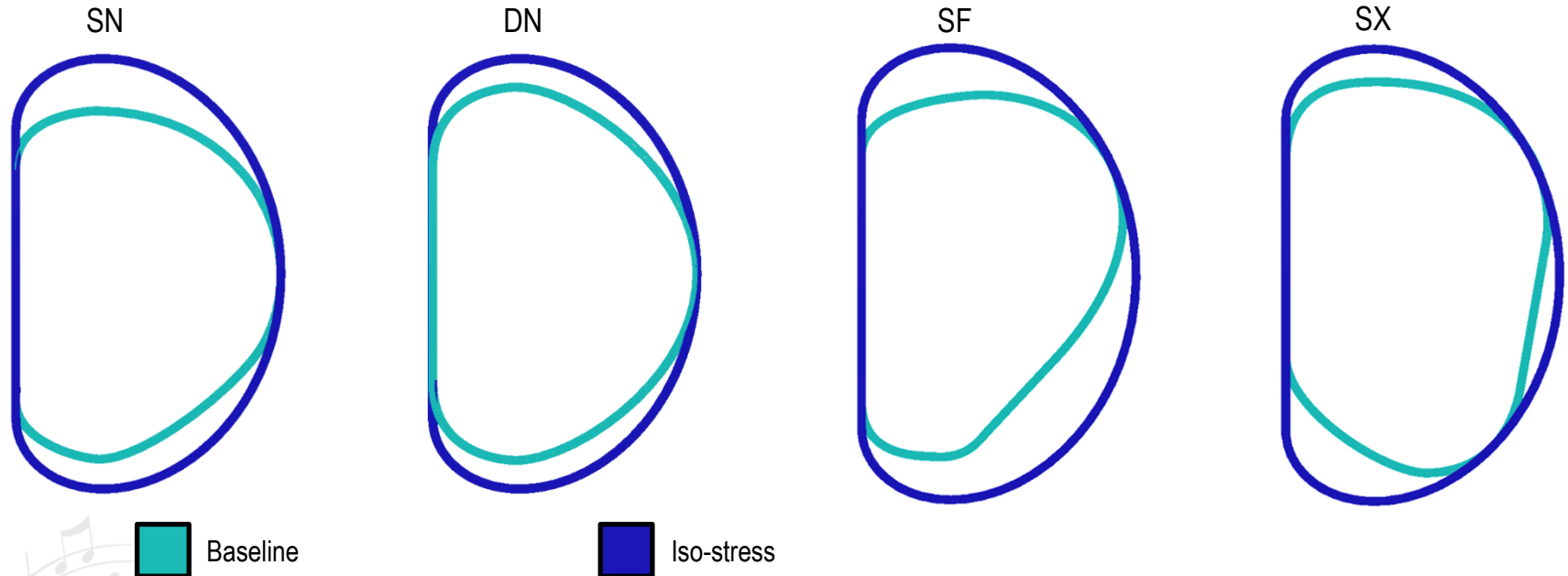
Iso-stress shape of the coil

- The optimal shape of a coil, structurally, has membrane stresses only when loaded
- Optimal iso-stress design has radius of curvature proportional to the radial coordinate at each point on the coil track*
- We can imagine for each ADC configuration an iso-stress profile, with the constraint of being always external and tangential wrt baseline

*Knoepfel, Heinz E. 2000. 'Magnetic fields: a comprehensive theoretical treatise for practical use'. John Wiley & Sons, New York, pp. 423-427

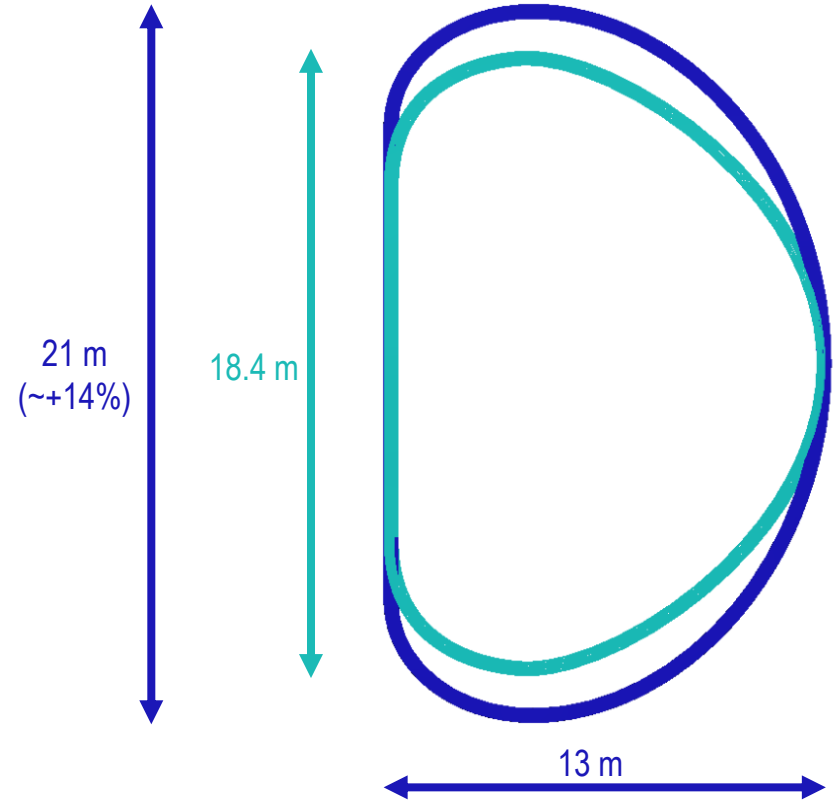
Iso-stress shape of the coil

- Iso-stress shape is symmetric with respect to the horizontal plane



Bending-free design of the coils

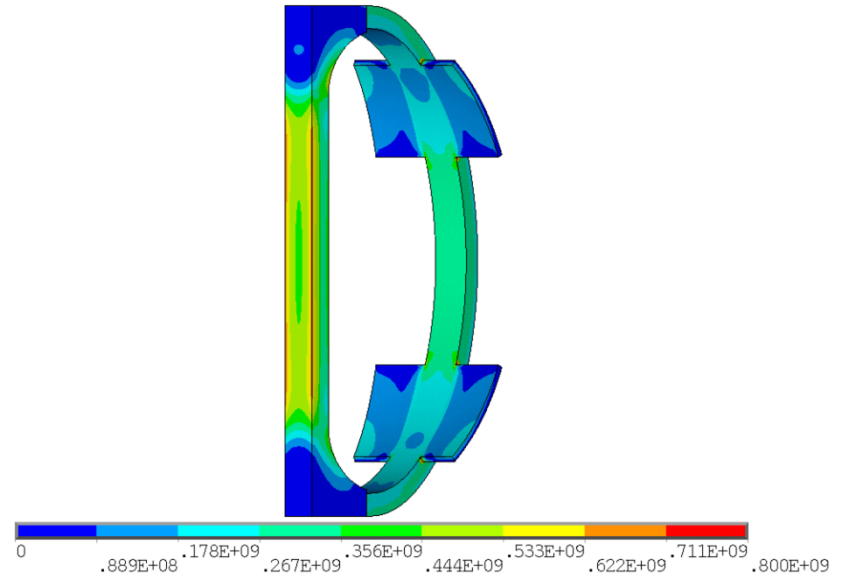
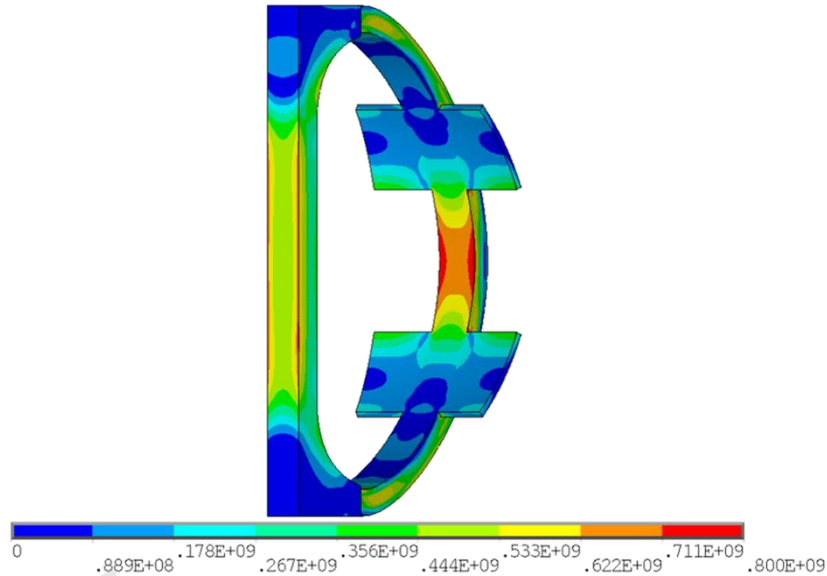
- Both configurations of the DN (baseline and bending-free) are perfectly symmetric wrt the horizontal plane
- Bending-free configuration is more elongated than the original one, being equal the radial size



Bending-free design of the coils

Baseline

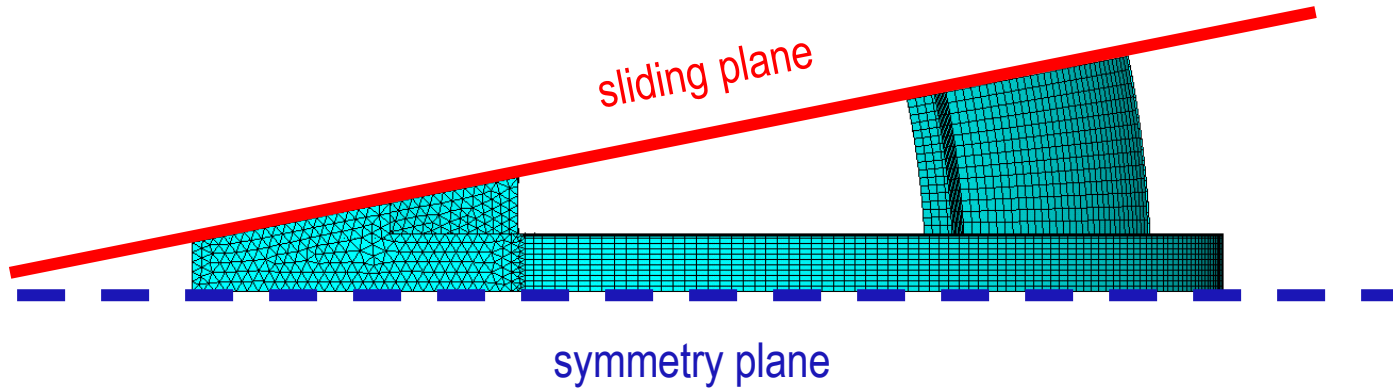
Bending-free



Optimisation Workflow: aim

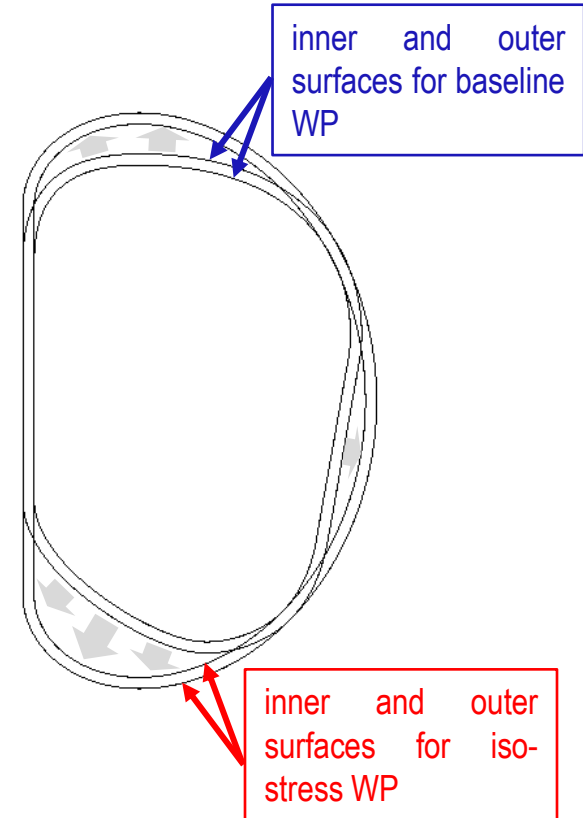
- Definition of a shape for the TF coils of the 4 cases (SN, DN, SF, SX) in-between the initial configuration and the iso-stress shape such to experience a stress state below a certain limit ($\sigma_{VM} = 450$ MPa) during magnetization
- A continuous transformation from the baseline to the iso-stress shape for each ADC case needs to be established
- A discrete number of TF coil configurations are extracted and considered for electromagnetic analysis (EM) and stress assessment

Optimisation Workflow: simplified model



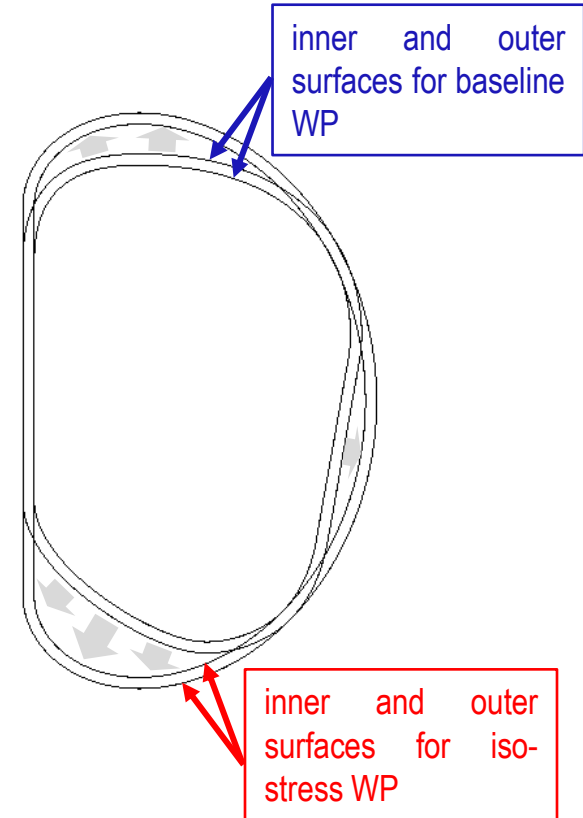
Optimisation Workflow: shape parameterisation

- WP inner and outer surfaces are considered for each pair baseline/iso-stress
- RBF Morph ACT Extension inside ANSYS Mechanical was used to perform shape parameterisation
- The displacement field shifting the first shape onto the second is applied to the whole TF structure (WP+casing+filler)



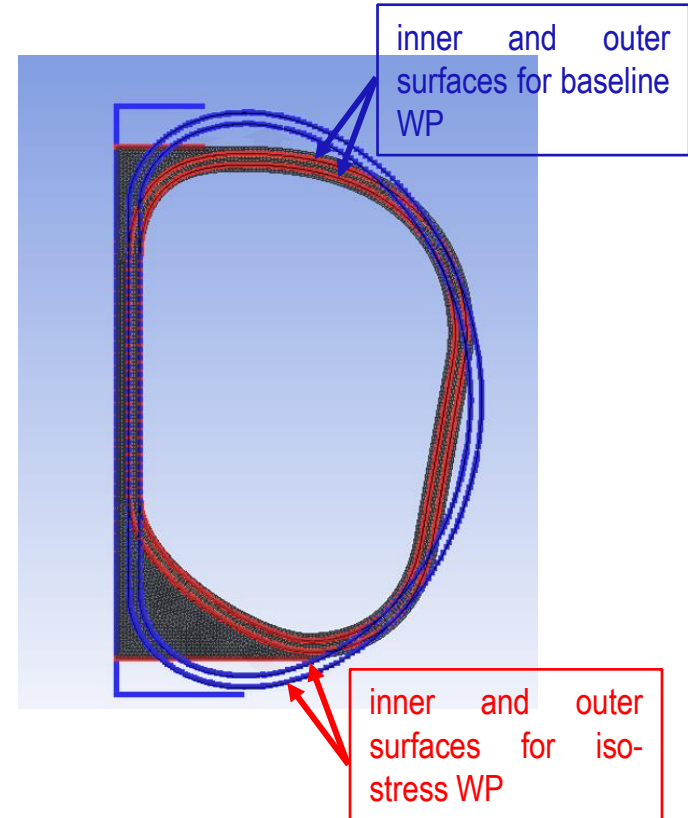
Optimisation Workflow: shape parameterisation

- A surface projection modifier was applied to each source-target pair
- The scaling of the defined displacement field determines the intermediate configurations in-between the initial shape and the iso-stress one (0 = baseline, 1 = iso-stress with steps of 0.1)



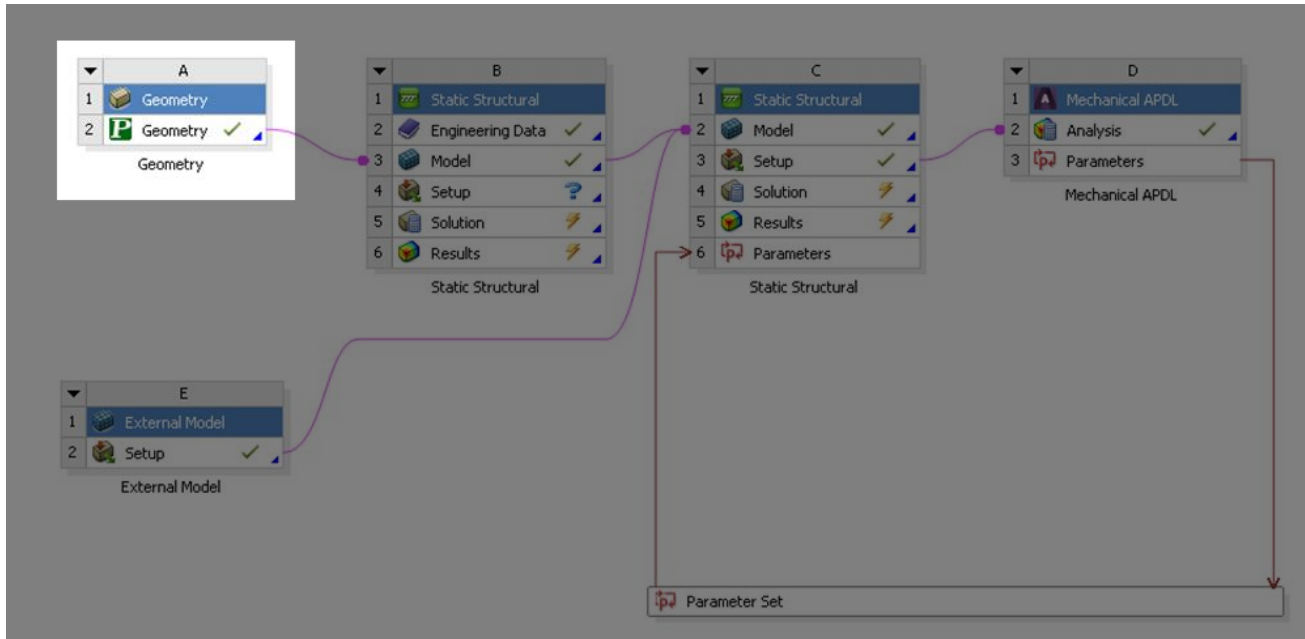
Optimisation Workflow: shape parameterisation

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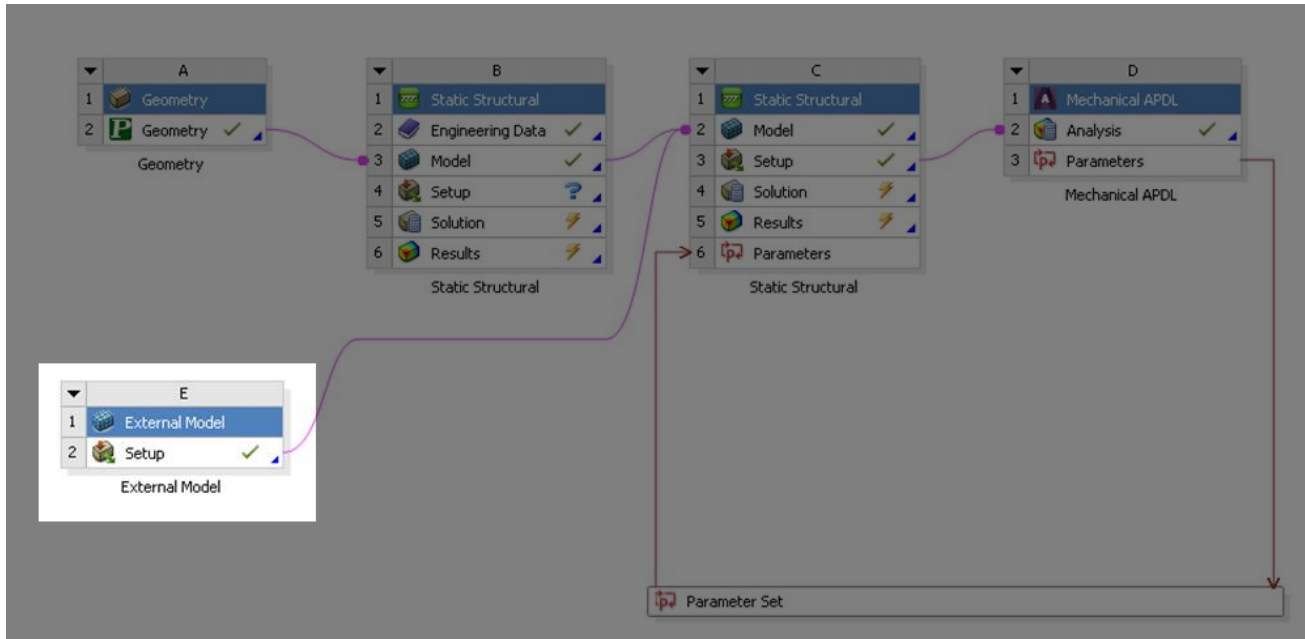
Optimisation Workflow

- Surface geometries are loaded from external CAD



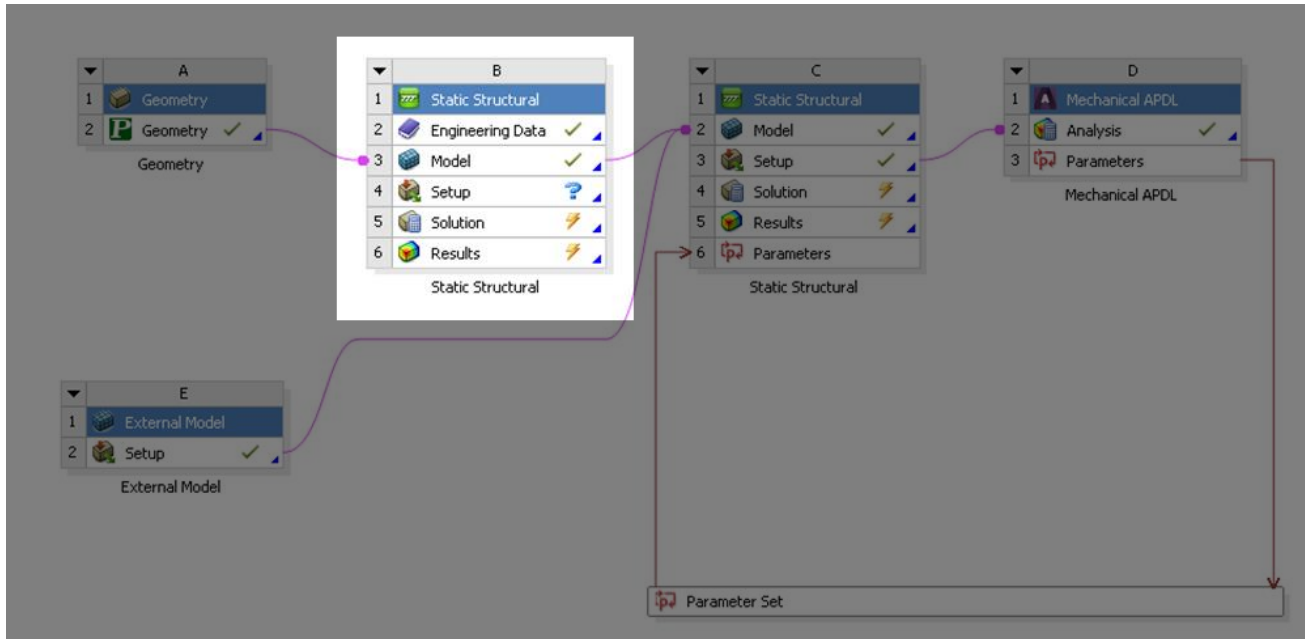
Optimisation Workflow

- Dead-mesh of the baseline model



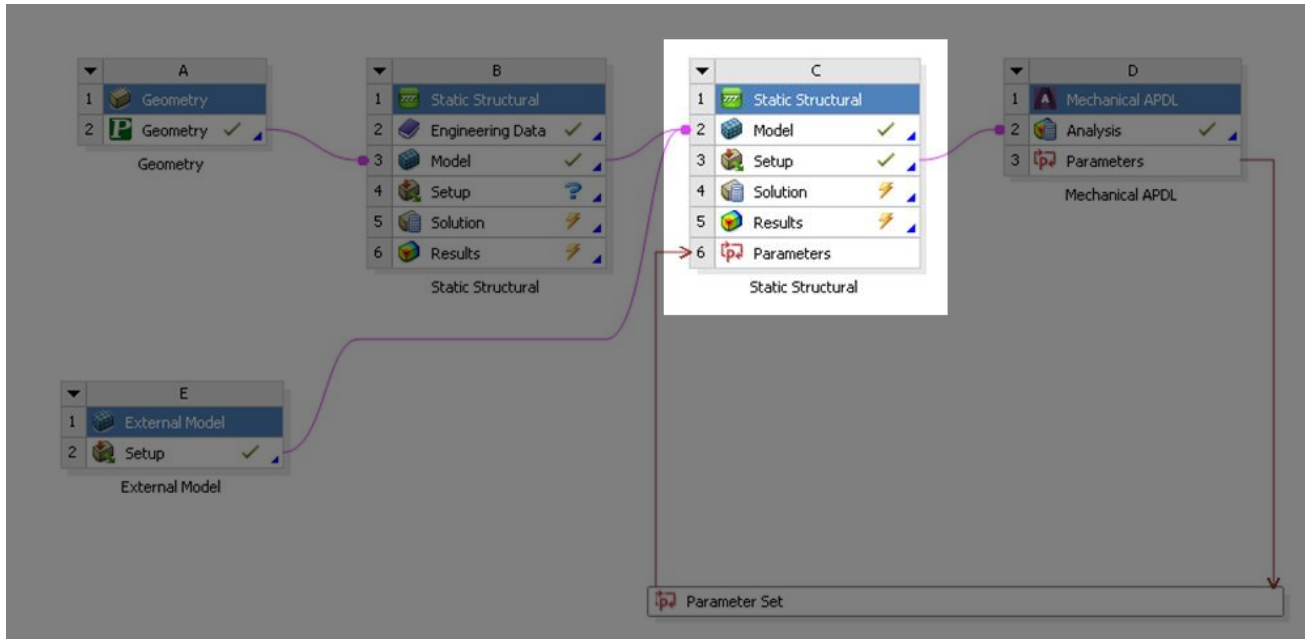
Optimisation Workflow

- Surfaces turned into ANSYS parametric geometries (meshed)



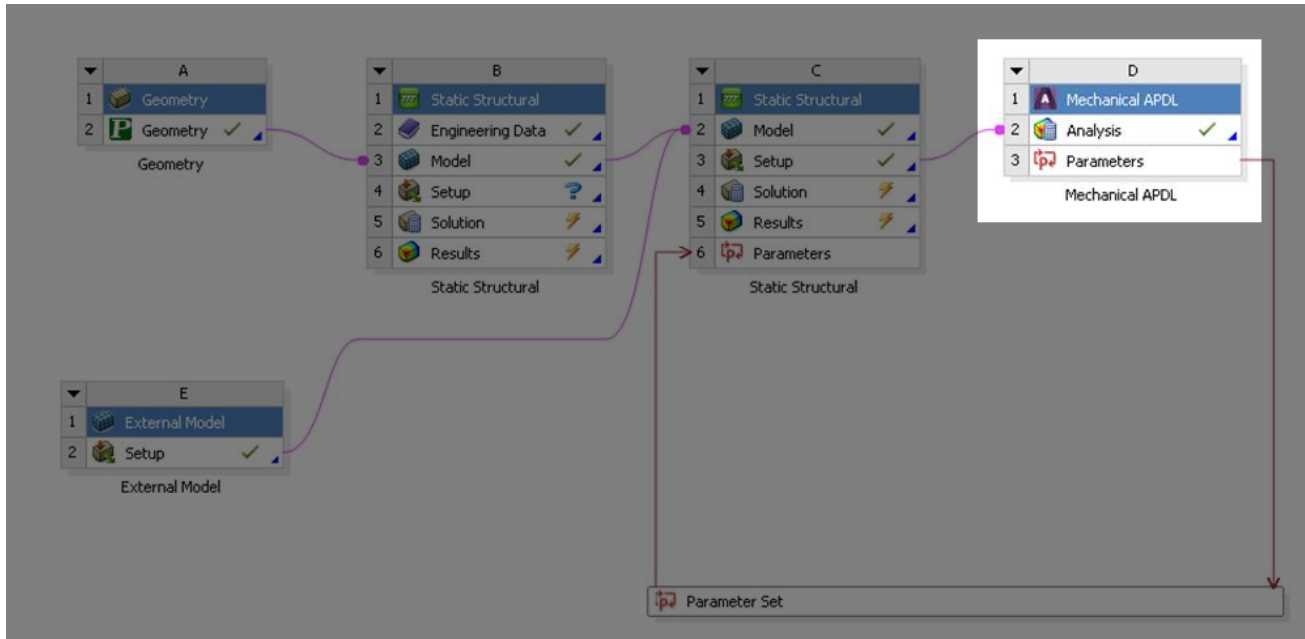
Optimisation Workflow

- RBFMorph modifies the model shape acting on nodal positions



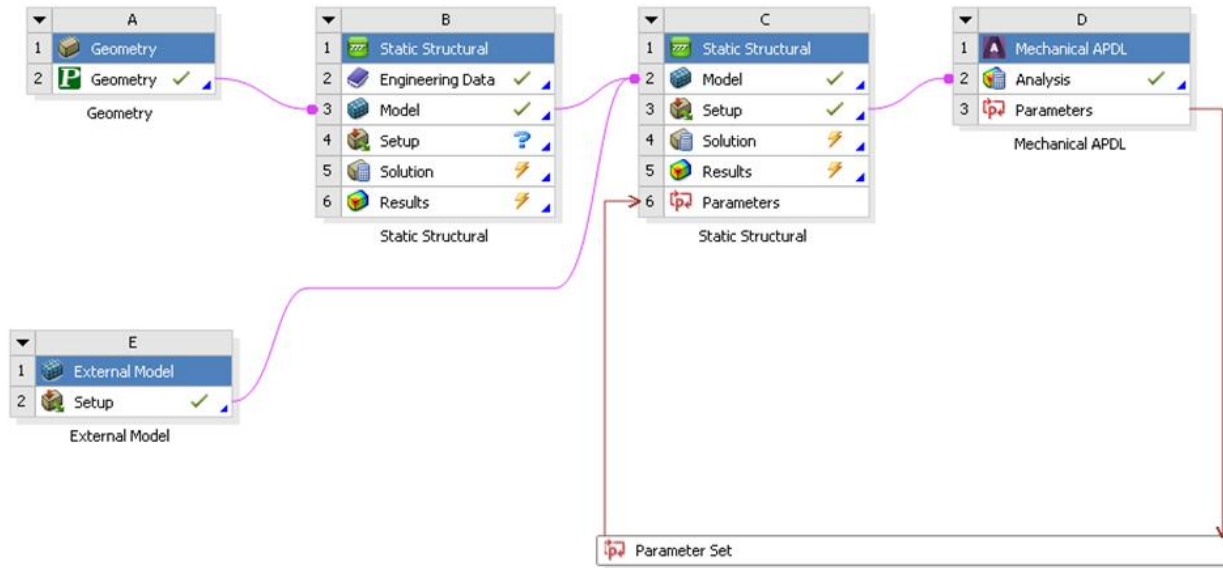
Optimisation Workflow

- Material assignment/orientation, EM analysis, structural analysis



Optimisation Workflow

- Optimisation is driven by DX, extracting stresses as output
- A DOE is calculated for each ADC configuration

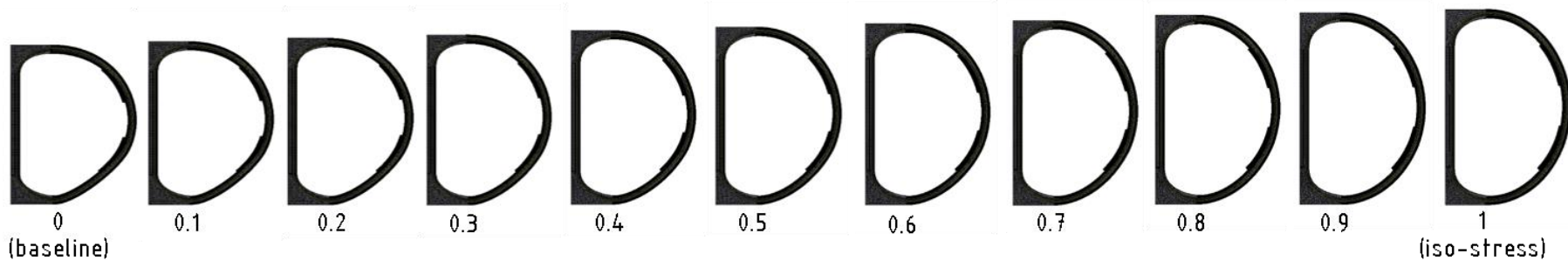


Optimisation Workflow: results

- Stress parameter σ_V introduced to evaluate optimisation, measuring the percentage of volume exceeding the chosen limit of 450 MPa of VM stress on casing
- Blending parameter between 0 (baseline) and 1 (iso-stress) is increased at intervals of 0.1
- Optimal shape for each ADC run is chosen to be the first with $\sigma_V \leq 1\%$
- Baseline σ_V values: 12%, 18%, 8%, 12%

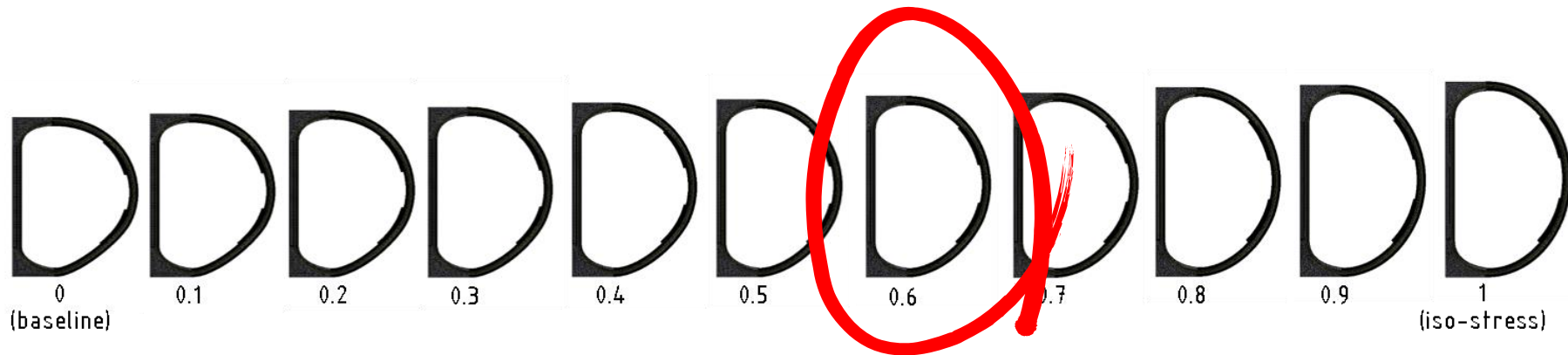
Automatic workflow: SN results

- Evolution of the SN from the baseline to the iso-stress configuration



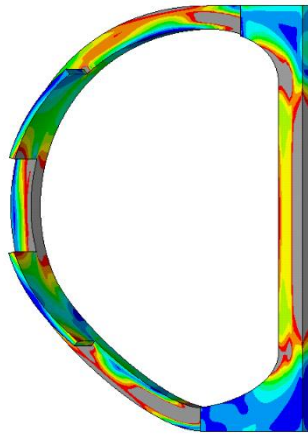
Automatic workflow: SN results

- Evolution of the SN from the baseline to the iso-stress configuration

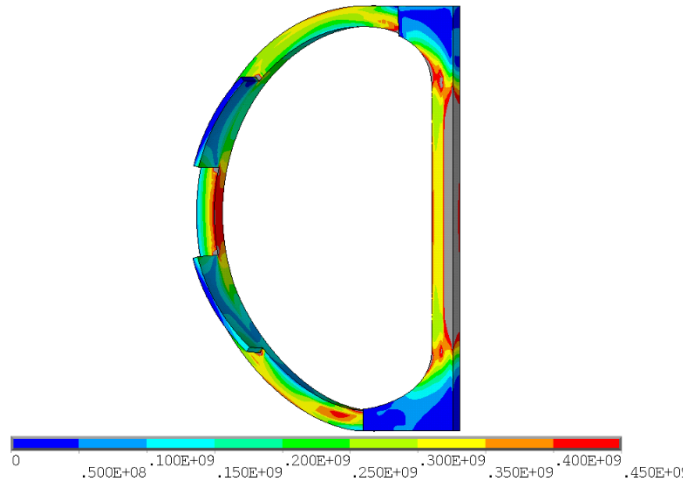


Automatic workflow: SN results

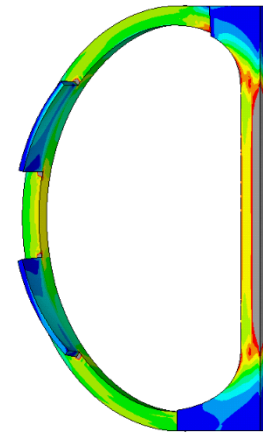
- Candidate shape with blending parameter 0.6
- Comparison with baseline and bending-free



Baseline, $H_{\text{casing}} = 17.6$ m



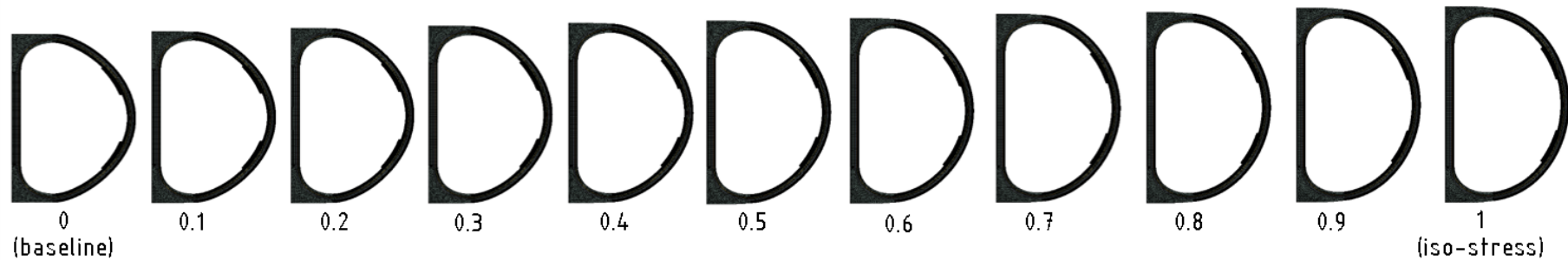
Candidate, $H_{\text{casing}} = 20.0$ m



Bending-free, $H_{\text{casing}} = 21.6$ m

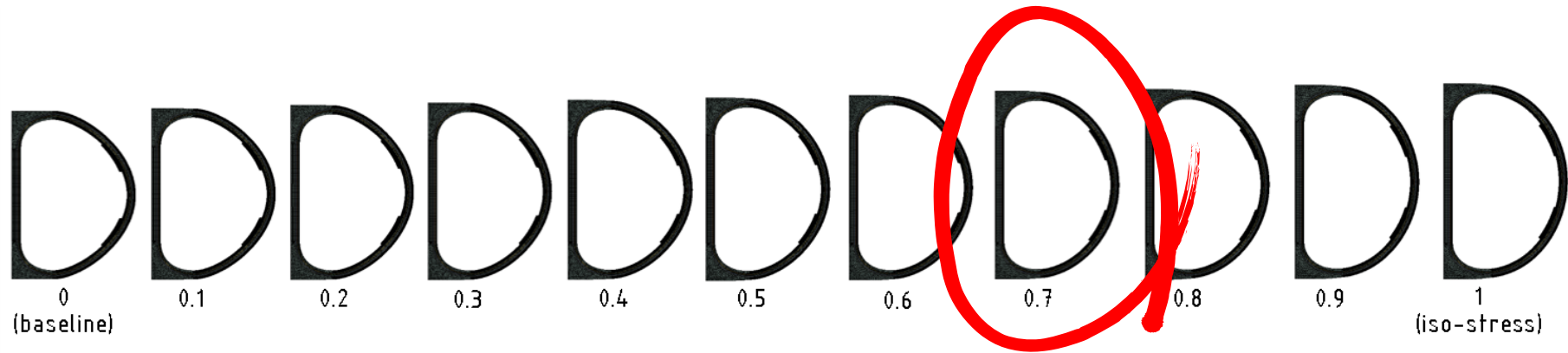
Automatic workflow: DN results

- Evolution of the DN from the baseline to the iso-stress configuration



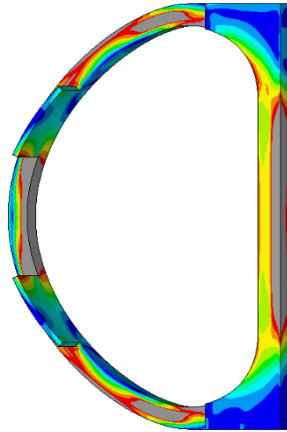
Automatic workflow: DN results

- Evolution of the DN from the baseline to the iso-stress configuration

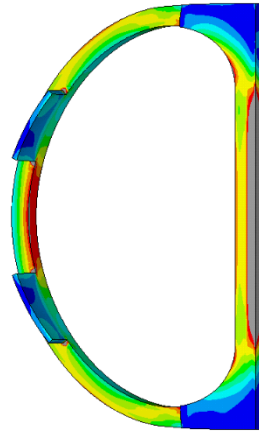


Automatic workflow: DN results

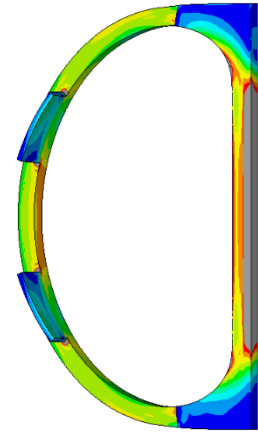
- Candidate shape with blending parameter 0.7
- Comparison with baseline and bending-free



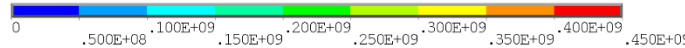
Baseline, $H_{\text{casing}}=18.9$ m



Candidate, $H_{\text{casing}}=21.1$ m

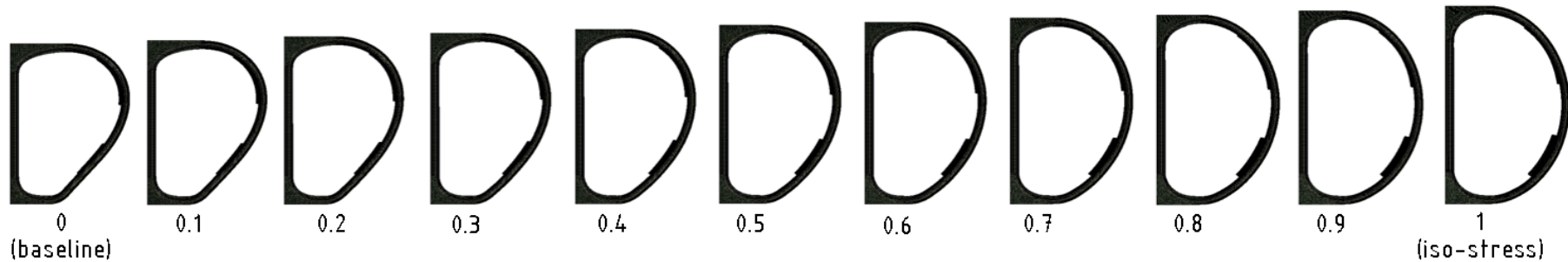


Bending-free, $H_{\text{casing}}=22.0$ m



Automatic workflow: SF results

- Evolution of the SF from the baseline to the iso-stress configuration



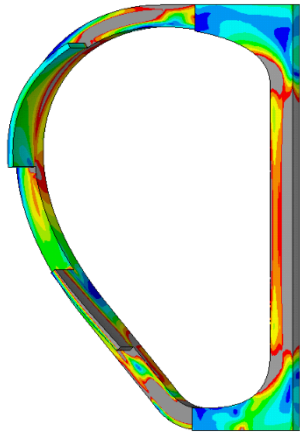
Automatic workflow: SF results

- Evolution of the SF from the baseline to the iso-stress configuration

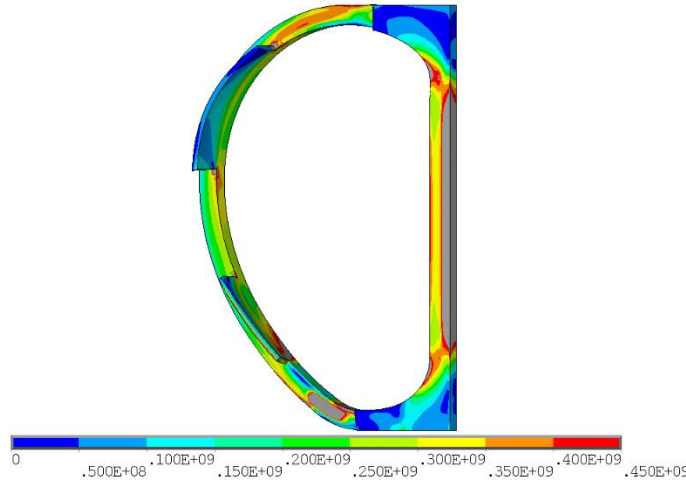


Automatic workflow: SF results

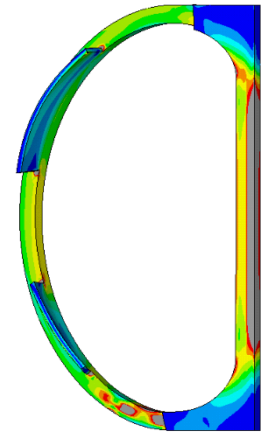
- Candidate shape with blending parameter 0.5
- Comparison with baseline and bending-free



Baseline, $H_{\text{casing}}=18.8$ m



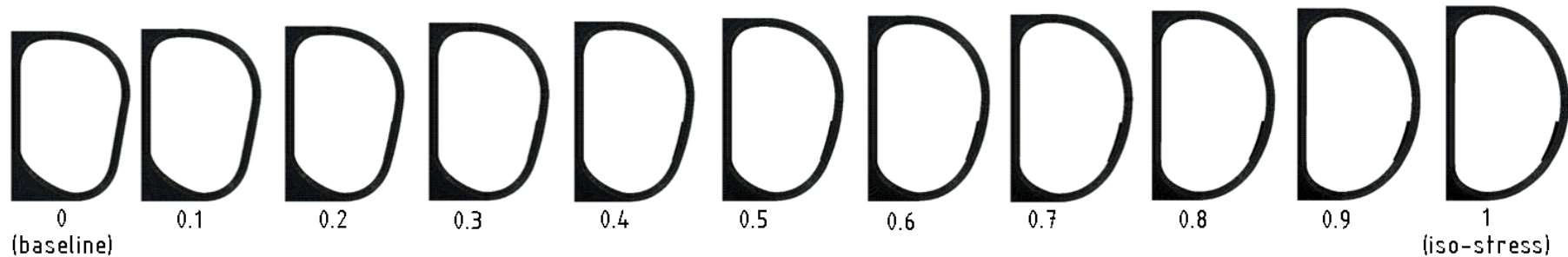
Candidate, $H_{\text{casing}}=21.0$ m



Bending-free, $H_{\text{casing}}=23.2$ m

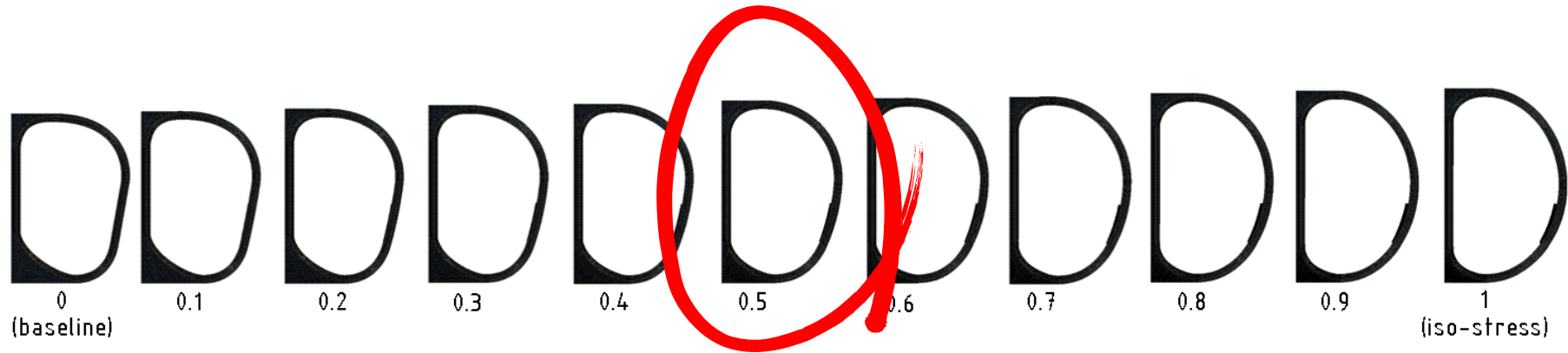
Automatic workflow: SX results

- Evolution of the SX from the baseline to the iso-stress configuration



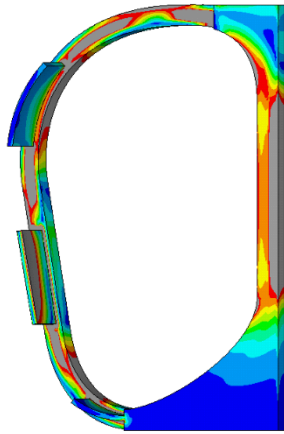
Automatic workflow: SX results

- Evolution of the SX from the baseline to the iso-stress configuration

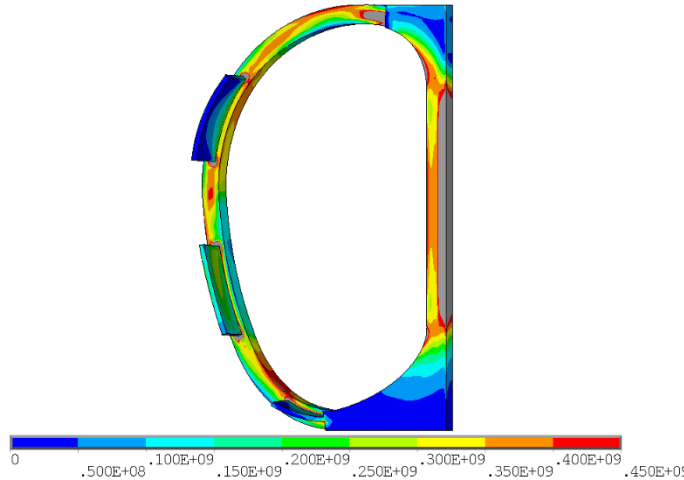


Automatic workflow: SX results

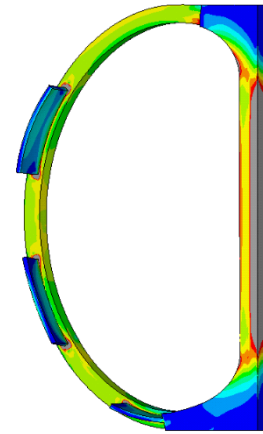
- Candidate shape with blending parameter 0.5
- Comparison with baseline and bending-free



Baseline, $H_{\text{casing}}=20.0$ m



Candidate, $H_{\text{casing}}=21.5$ m

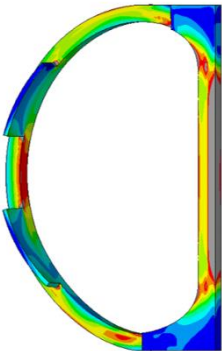
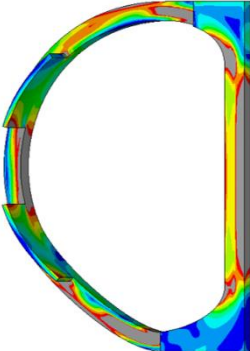


Bending-free, $H_{\text{casing}}=23.0$ m

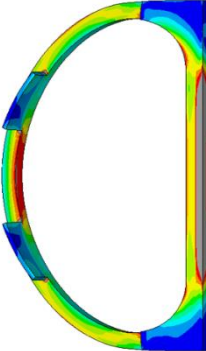
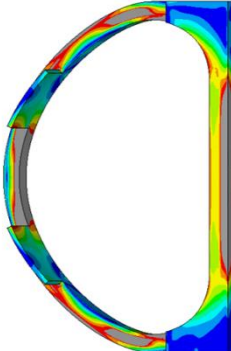
Results



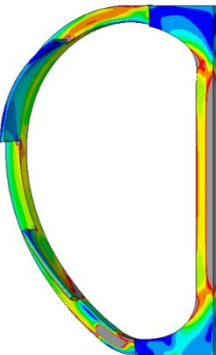
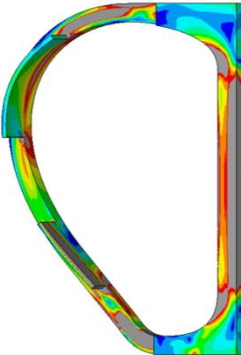
SN



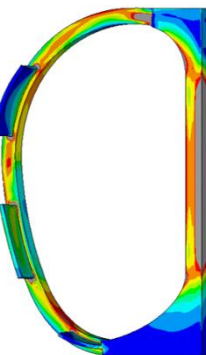
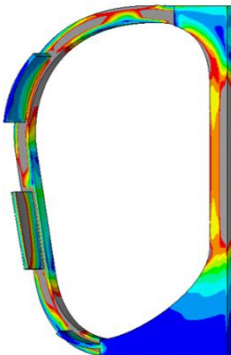
DN



SF



SX



Conclusions

- The SN candidate, computed on the simplified model, was explored on the full model, obtaining a satisfactory result
- The TF coils of the DEMO ADCs were originally designed to generate a magnetic field with specific characteristics, but not to withstand the Lorentz forces from EM interactions
- An optimization procedure based on ANSYS Workbench, RBF Morph and ANSYS APDL was built to find a compromise between their original shape and an iso-stress profile
- Proposed workflow was able to successfully find the minimum shape modification for each ADC in order to reduce the stress level to below 450 MPa

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