



# Optimization of industrial parts by mesh morphing enabled automatic shape sculpting

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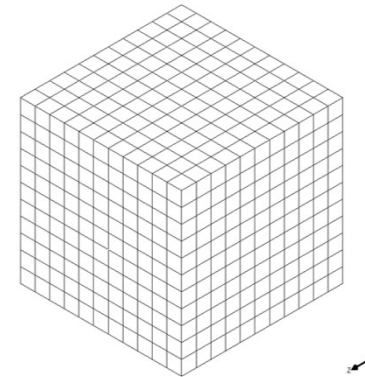


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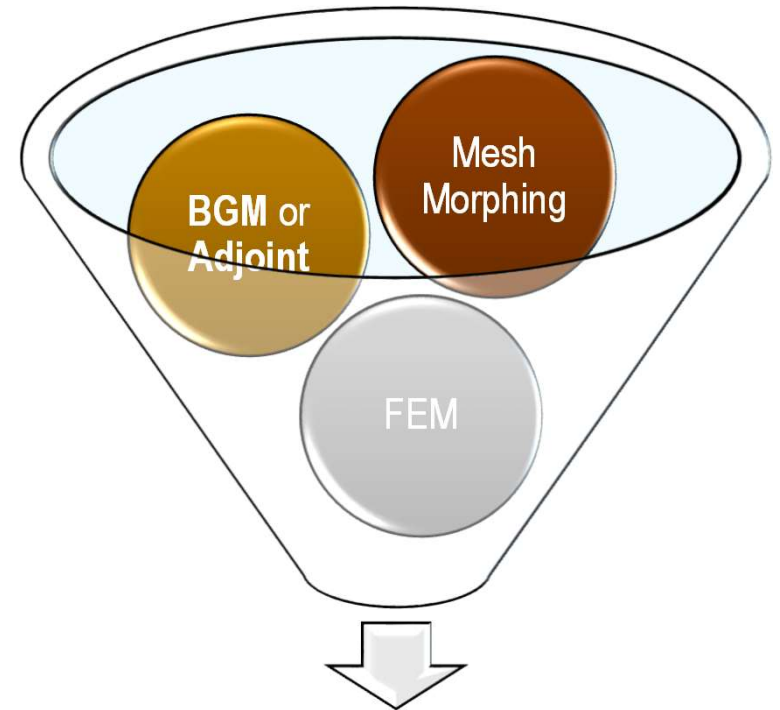
# Introduction

- Mechanical component **optimization** is a target for engineering applications.
- **Finite Element Method** is a tool for optimization given load and constraint configuration
- CAD based optimization requires the **generation of additional FEM models**. It can be very **time-consuming** specially dealing with complex shape components.
- To overcome this, **Mesh morphing** can be adopted:  
It generates new FEM models without modifying the geometry and without the need to remesh it.



# Introduction

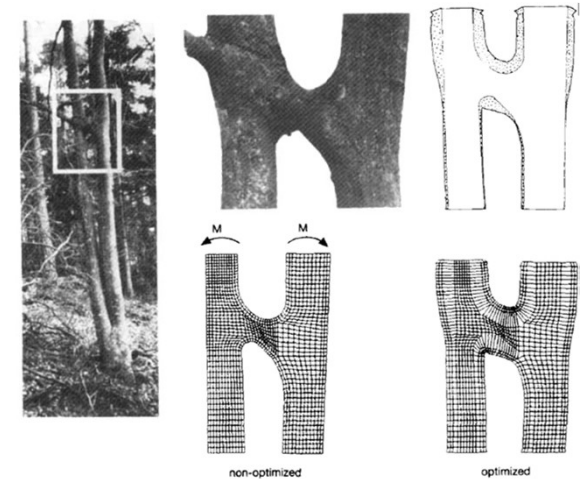
- **Biological Growth Method (BGM)** and **Adjoint Method** exploit data coming from numerical analysis to define a shape modification that will sculpt model surfaces so that **stress levels are optimized**.
- The tool adopted for morphing the **FEM** mesh is **RBF Morph™**, which is based on Radial Basis Functions (**RBFs**). FEM pre-processor and solver used is **ANSYS® Mechanical™**.



Automatic Shape optimization

# BGM Background

- **BGM\*** approach is based on the observation that **biological** structures growth is driven by **local** level of **stress**.
- Bones and trees' trunks are able to **adapt the shape** to mitigate the stress level due to external loads.
- The process is driven by stress **value at surfaces**. **Material** can be **added or removed** according to local values.



Reduction of maximum stresses 56 %



- The BGM idea is that surface growth can be expressed as a linear law with respect to a given threshold value:  $\dot{\epsilon} = k(\sigma_{Mises} - \sigma_{ref})$

\*Mattheck C., Burkhardt S., 1990. A new method of structural shape optimization based on biological growth. Int. J. Fatigue 12(3):185-190.

# BGM Background

- Waldman and Heller\* refined this first approach proposing a **multi peak** one:

$$d_i^j = \left( \frac{\sigma_i^j - \sigma_i^{th}}{\sigma_i^{th}} \right) \cdot s \cdot c, \quad \sigma_i^{th} = \max(\sigma_i^j) \text{ if } \sigma_i^j > 0 \quad \text{or} \quad \sigma_i^{th} = \min(\sigma_i^j) \text{ if } \sigma_i^j < 0$$

- In **RBF Morph ANSYS Workbench ACT** a different implementation is present

$$S_{node} = \frac{\sigma_{node} - \sigma_{th}}{\sigma_{max} - \sigma_{min}} \cdot d$$

and different **stress types** can be used to modify the surface shape:

- Von Mises stress
- Maximum principal stress
- Minimum principal stress
- Stress intensity
- Maximum Shear stress
- Equivalent plastic strain

\*Waldman W., Heller M., 2015. Shape optimization of holes in loaded plates by minimization of multiple stress peaks, Defence Science and Technology Organisation Fisherman Bend, Australia

# Adjoint Background

- **Adjoint method** allows to obtain the **sensitivities** of an **objective function** with respect to a set of **input parameters**.
- This can be applied to the three displacement for each node of the computational mesh, so that a **shape modification** can be obtained.
- Largely used in Computational Fluid-Dynamics (CFD) but can be also applied in Computational Structural Mechanics (CSM).
- It is possible to differentiate the discretised equation (**Discrete Adjoint method**) or to derive equation prior to their differentiation (**Continuous Adjoint method**).



# Adjoint Background (discrete case)

- The objective function can be expressed as function of displacement and the derivative:

$$\Psi = f(\mathbf{X}(u), u) \qquad \frac{d\Psi}{du} = \frac{\partial\Psi}{\partial u} + \frac{\partial\Psi}{\partial\mathbf{X}} \frac{\partial\mathbf{X}}{\partial u}$$

- To obtain the displacement  $\frac{\partial\mathbf{X}}{\partial u}$  two methods are available:
  - **direct method** → has to be re-evaluated for each input parameter)
  - **adjoint method** → need only one calculation no matter how many input parameters, it uses a Lagrange-like multiplier to obtain displacements:

$$\mathbf{K}\mathbf{X} = \mathbf{F} \quad \longrightarrow \quad \mathbf{K}\lambda = \frac{\partial\Psi^T}{\partial\mathbf{X}} \quad \longrightarrow \quad \frac{d\Psi}{du} = \frac{\partial\Psi}{\partial u} + \lambda^T \left( \frac{\partial\mathbf{F}}{\partial u} - \mathbf{X} \frac{\partial\mathbf{K}}{\partial u} \right)$$

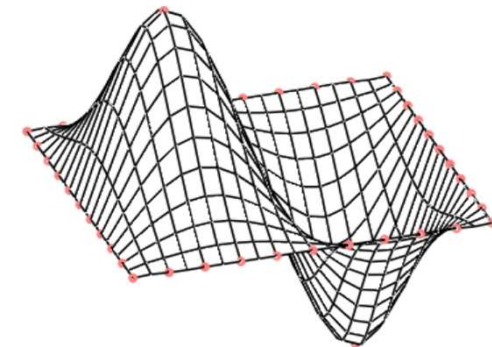
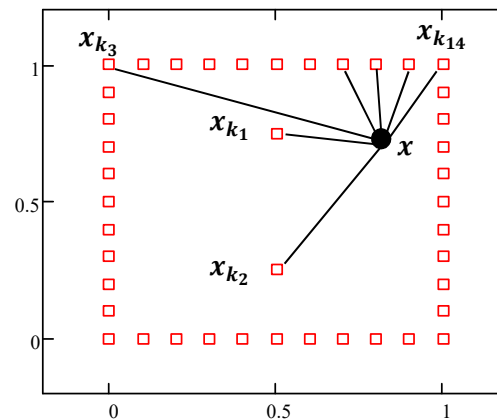


# RBF Background

- RBFs = mathematical tool capable to **interpolate** in a generic point in the space a function **known** in a discrete set of points (**source points**).
- The interpolating function is composed by a **radial basis** and by a **polynomial**:



$$s(\mathbf{x}) = \sum_{i=1}^N \underbrace{\gamma_i \varphi(\underbrace{\|\mathbf{x} - \mathbf{x}_{k_i}\|}_{\text{distance from the } i\text{-th source point}})}_{\text{radial basis}} + \underbrace{h(\mathbf{x})}_{\text{polynomial}}$$



# RBF Background

- If evaluated on the source points, interpolating function gives exactly the input values
- RBF problem (evaluation of coefficients  $\boldsymbol{\gamma}$  and  $\boldsymbol{\beta}$ ) is associated to the solution of a linear system:
  - $\mathbf{M}$  = interpolation matrix
  - $\mathbf{P}$  = constraint matrix
  - $\mathbf{g}$  = vector of known values on the source points
- Once solved the RBF problem each displacement component is interpolated

$$\begin{bmatrix} \mathbf{M} & \mathbf{P} \\ \mathbf{P}^T & \mathbf{0} \end{bmatrix} \begin{pmatrix} \boldsymbol{\gamma} \\ \boldsymbol{\beta} \end{pmatrix} = \begin{pmatrix} \mathbf{g} \\ \mathbf{0} \end{pmatrix}$$

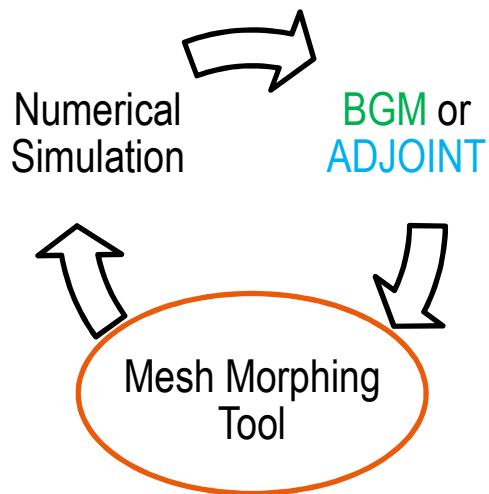
$$M_{ij} = \varphi(\mathbf{x}_{k_i} - \mathbf{x}_{k_j}) \quad 1 \leq i, j \leq N$$

$$\mathbf{P} = \begin{bmatrix} 1 & x_{k_1} & y_{k_1} & z_{k_1} \\ 1 & x_{k_2} & y_{k_2} & z_{k_2} \\ \vdots & \vdots & \vdots & \vdots \\ 1 & x_{k_N} & y_{k_N} & z_{k_N} \end{bmatrix}$$

$$\begin{cases} s_x(\mathbf{x}) = \sum_{i=1}^N \gamma_i^x \varphi(\mathbf{x} - \mathbf{x}_{k_i}) + \beta_1^x + \beta_2^x x + \beta_3^x y + \beta_4^x z \\ s_y(\mathbf{x}) = \sum_{i=1}^N \gamma_i^y \varphi(\mathbf{x} - \mathbf{x}_{k_i}) + \beta_1^y + \beta_2^y x + \beta_3^y y + \beta_4^y z \\ s_z(\mathbf{x}) = \sum_{i=1}^N \gamma_i^z \varphi(\mathbf{x} - \mathbf{x}_{k_i}) + \beta_1^z + \beta_2^z x + \beta_3^z y + \beta_4^z z \end{cases}$$

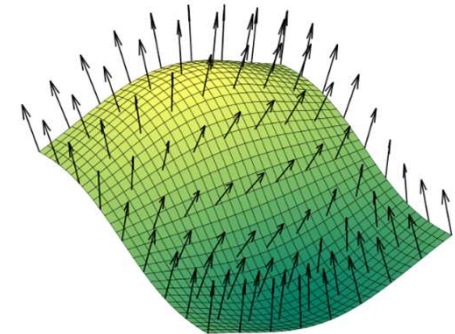
# Automatic Surface Sculpting

- **Automatic** optimization is accomplished connecting **BGM** or **ADJOINT** data from numerical simulation to mesh morphing tool.



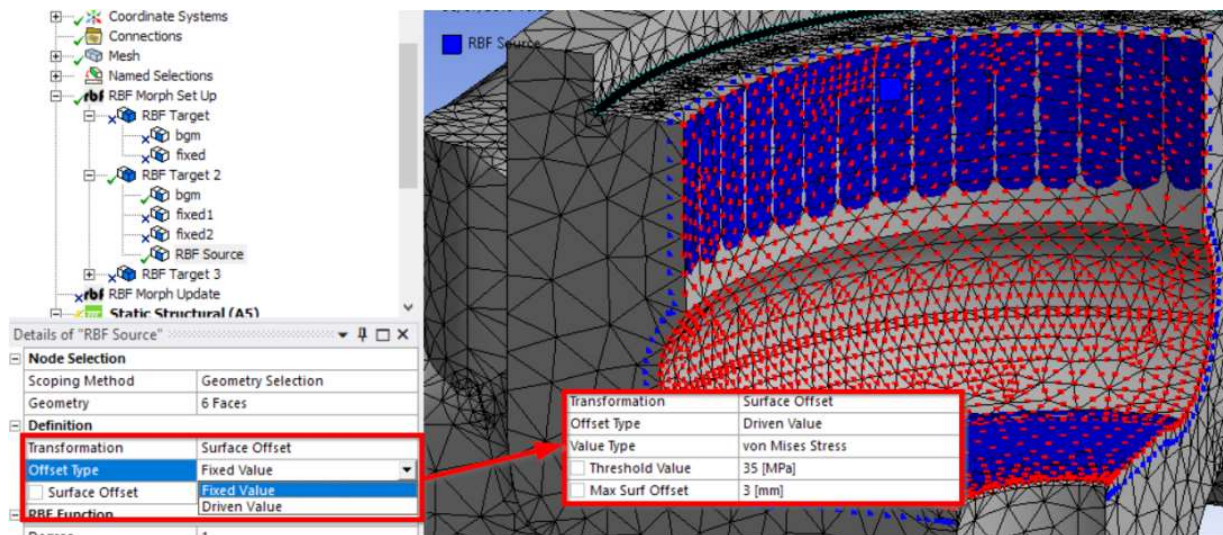
## Offset Surface

each node can displace according to the **local normal direction**



# Automatic Surface Sculpting - BGM

- Direction and amplitude of displacement is defined according to **stress data**, considering the threshold stress value  $\sigma_{th}$  and the  $d$  maximum displacement.

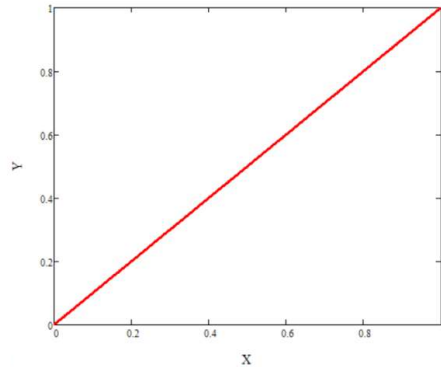


$$S_{node} = \frac{\sigma_{node} - \sigma_{th}}{\sigma_{max} - \sigma_{min}} \cdot d$$

# Automatic Surface Sculpting - Adjoint

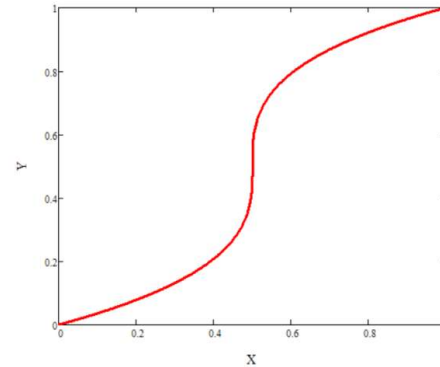
- Direction and amplitude of displacement is defined according to **topological optimization** data, considering the topological density function,  $\rho \in [0,1]$ , interpolated using a linear or irrational function and the  $d$  maximum displacement.

linear



$$S_{node\ adj} = [(\rho - 0.5) + 0.5] \cdot d$$

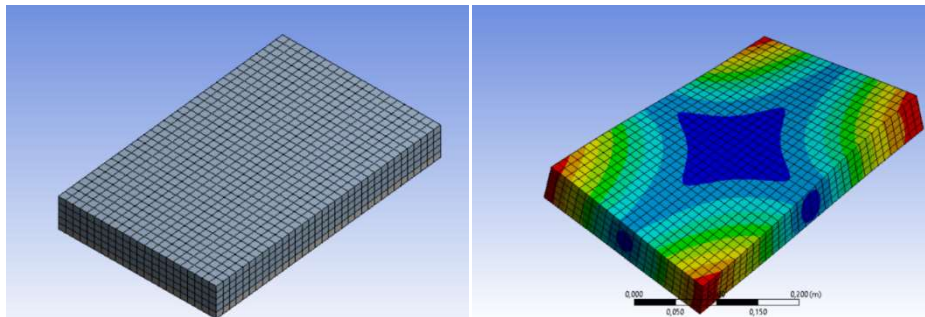
irrational



$$S_{node\ adj} = \left[ 0.5 \left( \frac{(\rho - 0.5)}{0.5} \right)^{\frac{1}{3}} + 0.5 \right] \cdot d, \quad \text{with } \rho \in [0, 1]$$

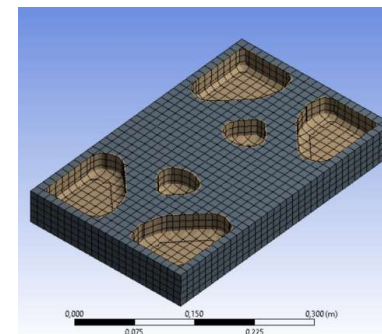
# Applications – Simple Thick Plate – Adjoint

- Free and undamped dynamic analysis of a thick plate



Mode	Freq. (Hz)
1	1457
2	1542
3	3159
4	3800
5	3816

- Optimization problem:
  - decrease mass (target -50%)
  - maintain first frequency above 1220 Hz



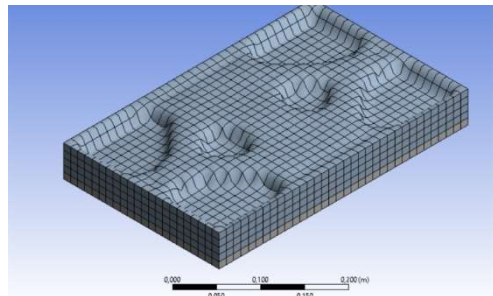
Topology  
Optimization  
Result

↓

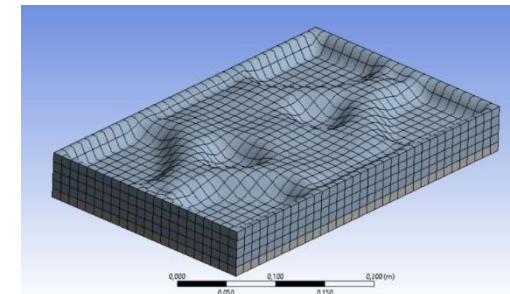
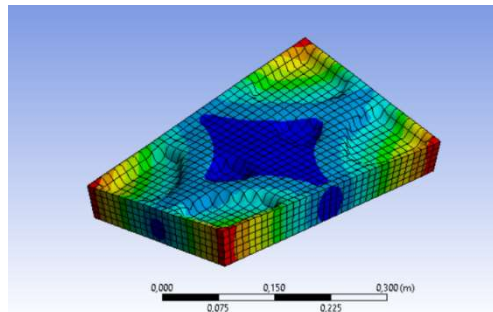
input for adjoint

# Applications – Simple Thick Plate – Adjoint

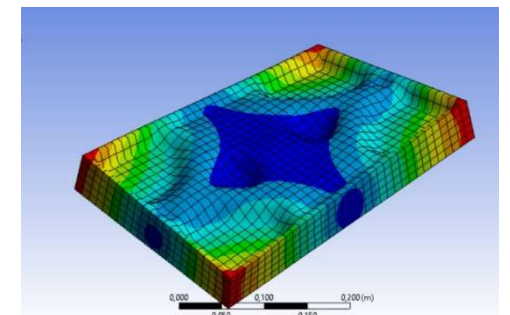
Results ( $d = 15\text{mm}$ )



Irrational Interpolation



Linear Interpolation



Mode	Baseline Freq. (Hz)	Linear int. Freq. (Hz)	Irrational int. Freq. (Hz)
1	1457	1316	1352
2	1542	1402	1441
...	...	...	...

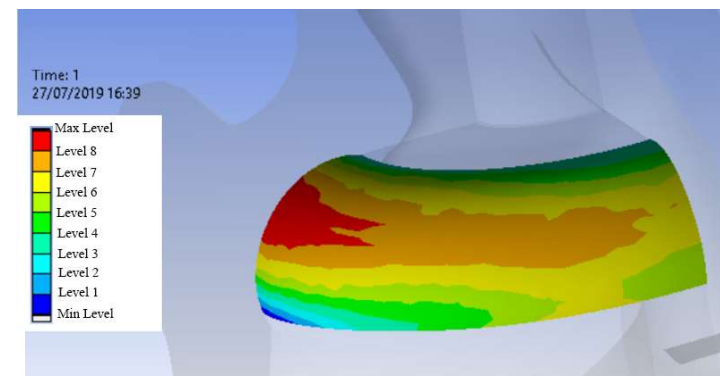
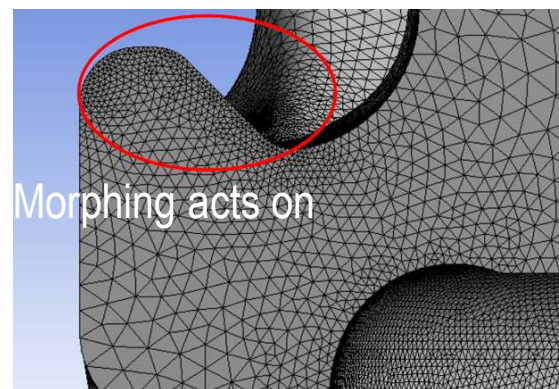
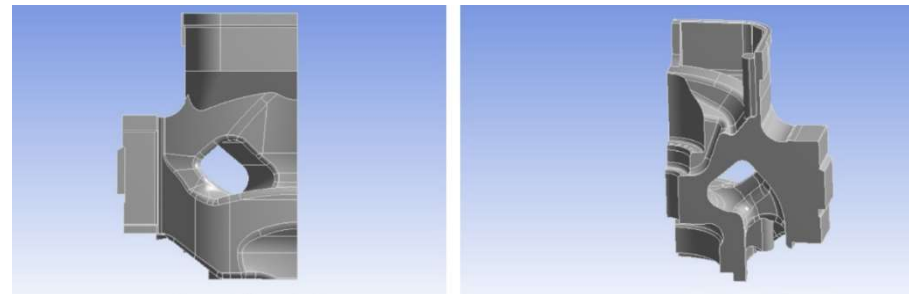
Mass reduction = 20% (< 50%)

Topological Optimization removes material  
→ mesh morphing moves nodes.



# Applications – Industrial component – Adjoint

- Maximum reference stress reduction: **11.7 %**



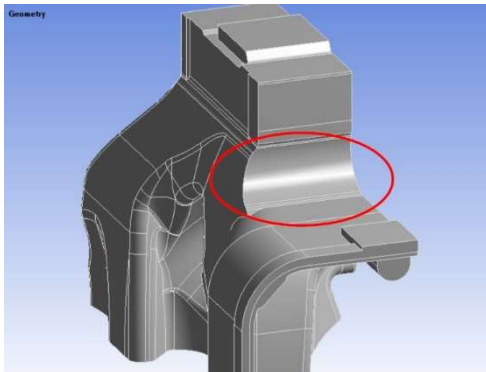


# Applications – Industrial component – BGM

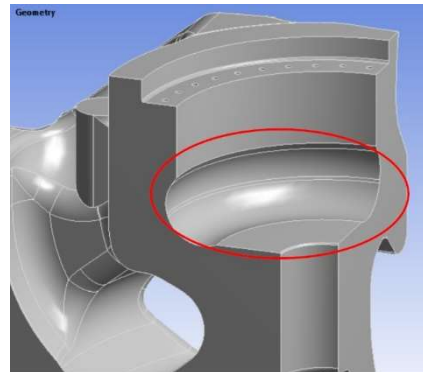
- 3 Hot Spots identified

Location	$\sigma_{th}$	$d$ [mm]
Hot Spot 1	$0.5(\sigma_{max}-\sigma_{min})$	3
Hot Spot 2	$0.5(\sigma_{max}-\sigma_{min})$	3
Hot Spot 3	$0.5(\sigma_{max}-\sigma_{min})$	1

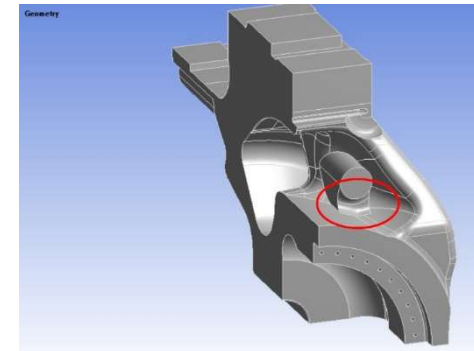
$$S_{node} = \frac{\sigma_{node} - \sigma_{th}}{\sigma_{max} - \sigma_{min}} \cdot d$$



Hot Spot 1



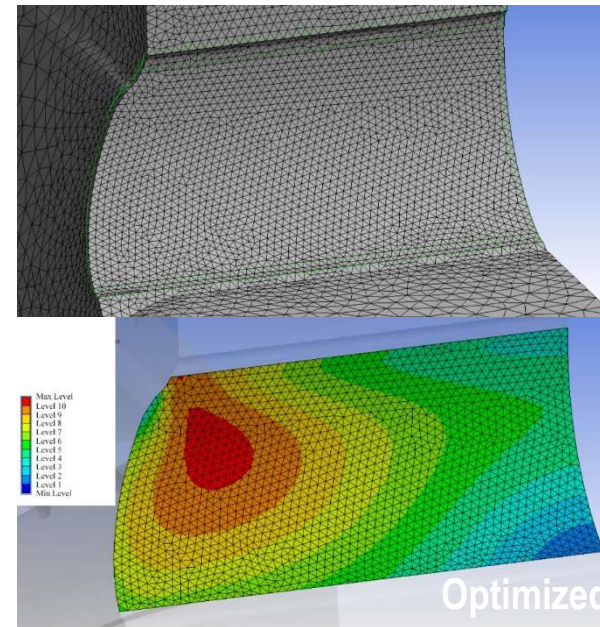
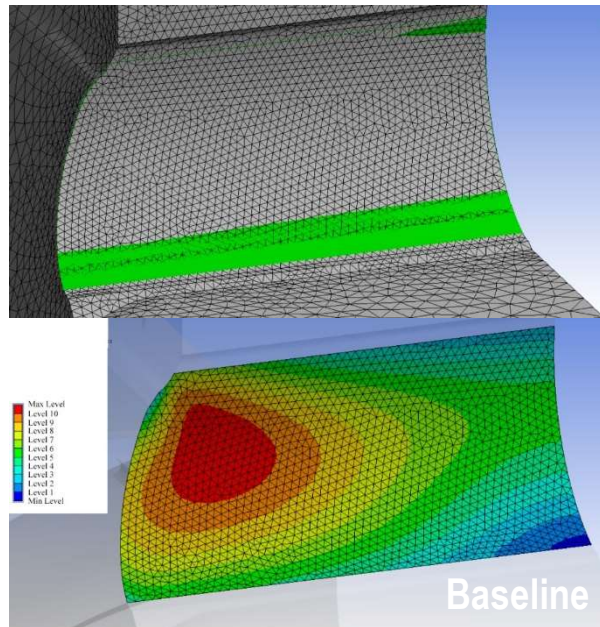
Hot Spot 2



Hot Spot 3

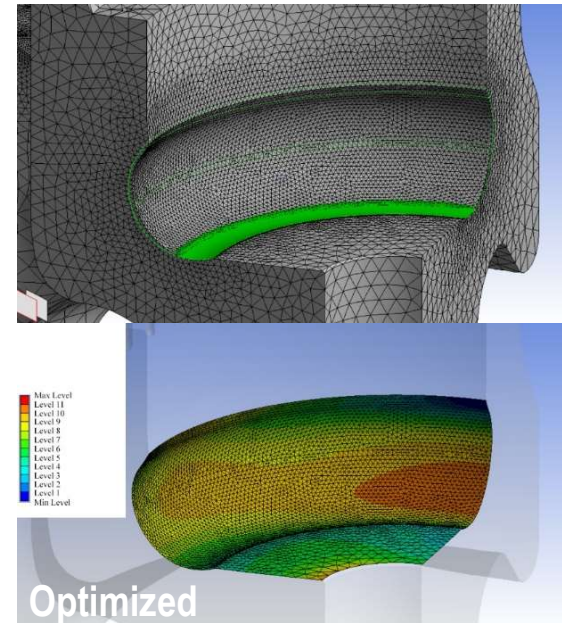
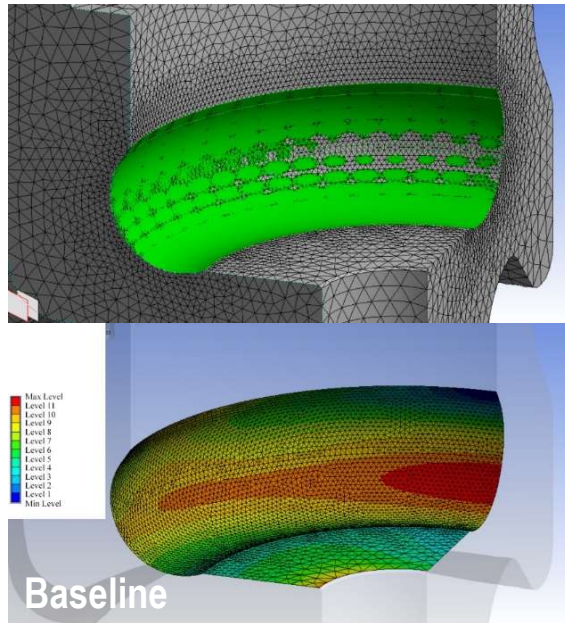
# Applications – Industrial component – BGM

- Hot Spot 1
- Max stress reduction: **2.76%**



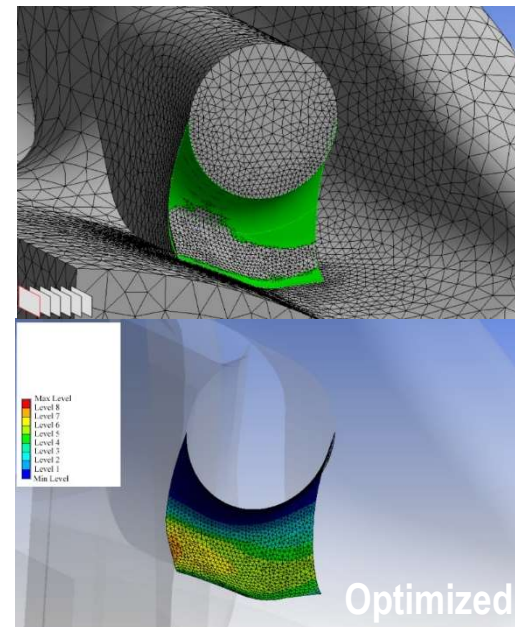
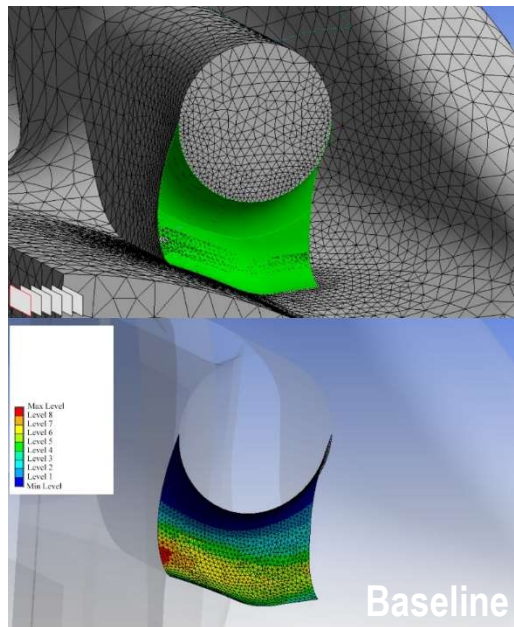
# Applications – Industrial component – BGM

- Hot Spot 2
- Max stress reduction: **7.85%**



# Applications – Industrial component – BGM

- Hot Spot 3
- Max stress reduction: **8.12%**



# Conclusions

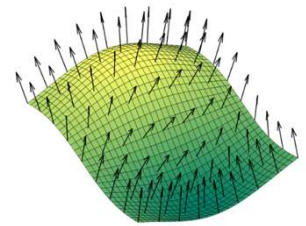
- A methodology to perform automatic shape optimization via surface sculpting was presented.
- Two approaches were investigated **Biological Growth Method** and **Adjoint Method**, which were successfully coupled with mesh morphing tool.
- **Adjoint** method, at the cost of an additional computation, gives sensitivities with respect of objective functions which were used to identify surface nodes to be moved inward or outward.
- **BGM** uses surfaces stress levels to identify model zones to be moved inward or outward, obtaining stress peak minimization and more uniform stress distribution





# Conclusions

- Both approaches were illustrated on **simple geometries** and then applied to a more **complex case**.
- The proposed procedure allowed to reach **optimized shapes** matching different **objective functions** in an **automatic way**, with a **minimal effort from the user**.
- The framework adopted was composed by ANSYS Workbench with RBF Morph ACT extension, which provided an integrated tool to the user in which perform optimization task





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